



# LhARA: The Laser-hybrid Accelerator for Radiobiological Applications

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## 2 ABSTRACT

3 The 'Laser-hybrid Accelerator for Radiobiological Applications', LhARA, is conceived as a novel,  
4 flexible facility dedicated to the study of radiobiology. The technologies demonstrated in LhARA,  
5 which have wide application, will be developed to allow particle-beam therapy to be delivered in  
6 a new regimen, combining a variety of ion species in a single treatment fraction and exploiting  
7 ultra-high dose rates. LhARA will be a hybrid accelerator system in which laser interactions drive  
8 the creation of a large flux of protons or light ions that are captured using a plasma (Gabor)  
9 lens and formed into a beam. The laser-driven source allows protons and ions to be captured  
10 at energies significantly above those that pertain in conventional facilities, thus evading the  
11 current space-charge limit on the instantaneous dose rate that can be delivered. The laser-hybrid  
12 approach, therefore, will allow the radiobiology that determines the response of tissue to ionising  
13 radiation to be studied with protons and light ions using a wide variety of time structures, spectral  
14 distributions, and spatial configurations at instantaneous dose rates up to and significantly beyond  
15 the ultra-high dose-rate 'FLASH' regime.

16 It is proposed that LhARA be developed in two stages. In the first stage, a programme of *in vitro*  
17 radiobiology will be served with proton beams with energies between 10 MeV and 15 MeV. In  
18 stage two, the beam will be accelerated using a fixed-field alternating-gradient accelerator (FFA).  
19 This will allow experiments to be carried out *in vitro* and *in vivo* with proton beam energies of up  
20 to 127 MeV. In addition, ion beams with energies up to 33.4 MeV per nucleon will be available for  
21 *in vitro* and *in vivo* experiments. This paper presents the conceptual design for LhARA and the  
22 R&D programme by which the LhARA consortium seeks to establish the facility.

## 23 LAY SUMMARY

24 It is well established that radiation therapy (RT) is an effective treatment for many types of cancer.  
25 Most treatments are delivered by machines that accelerate electrons which are then used to  
26 produce a beam of high-energy photons (X-rays) which are directed at a tumour to kill cancer  
27 cells. However, healthy tissue anywhere in the path of the photon beam is also irradiated and so  
28 can be damaged. Modern X-ray therapy is able to reduce this damage by using several beams at  
29 different angles.

30 Recent years have seen the use of a new type of machine in which protons are accelerated to  
31 produce proton beams (rather than photon beams) which are directed at a tumour. These proton  
32 beams can be arranged to deposit almost all of their energy in a small volume within a tumour so  
33 they cause little damage to healthy tissue; a major advantage over photon beams. But proton  
34 machines are large and expensive, so there is a need for the development of proton machines  
35 that are smaller, cheaper and more flexible in how they can be used.

36 The LhARA project is aimed at the development of such proton machines using a new approach  
37 based on high power lasers. Such new machines could also make it easier to deliver the dose in  
38 very short high-intensity pulses and as a group of micro-beams—exciting recent research has  
39 shown that this brings improved effectiveness in killing cancer cells while sparing healthy tissue.  
40 The technology to be proved in LhARA should enable a course of RT to be delivered in days  
41 rather than weeks.

42 Scientifically, there is a need to understand better the basic processes by which radiation  
43 interacts with biological matter to kill cancer cells—the investigation of these processes involves  
44 physics as well as biology. Thus the most important aim of LhARA is to pursue this radiobiological

45 research in new regimens and from this to develop better treatments. LhARA will also pursue  
46 technological research into laser-hybrid accelerators.

47 **Keywords:** Radiobiology, Novel acceleration, Proton beam therapy, Ion beam therapy, Laser-driven acceleration, Plasma lens, Fixed-  
48 field alternating-gradient acceleration

## 1 INTRODUCTION

49 Cancer is the second most common cause of death globally [The World Health Organisation (2020)]. In  
50 2018, 18.1 million new cancer cases were diagnosed, 9.6 million people died of cancer-related disease, and  
51 43.8 million people were living with cancer [Bray et al. (2018); Fitzmaurice et al. (2018)]. It is estimated  
52 that 26.9 million life-years could be saved in low- and middle-income countries if radiotherapy capacity  
53 could be scaled up [Atun et al. (2015)]. Novel techniques incorporated in facilities that are at once robust,  
54 automated, efficient, and cost-effective are required to deliver the required scale-up in provision.

55 Radiation therapy, a cornerstone of cancer treatment, is used in over 50 % of cancer patients [Datta et al.  
56 (2019)]. The most frequently used types of RT employ photon or electron beams with MeV-scale energies.  
57 Proton and ion beams offer substantial advantages over X-rays because the bulk of the beam energy is  
58 deposited in the Bragg peak. This allows dose to be conformed to the tumour while sparing healthy tissue  
59 and organs at risk. The benefits of proton and ion-beam therapy (PBT) are widely recognised. PBT today is  
60 routinely delivered in fractions of  $\sim 2$  Gy per day over several weeks; each fraction being delivered at a rate  
61 of  $\lesssim 5$  Gy/minute deposited uniformly over the target treatment volume. There is evidence of therapeutic  
62 benefit when dose is delivered at ultra-high rate,  $\gtrsim 40$  Gy/s, in “FLASH” RT [Berry (1973); Favaudon et al.  
63 (2014); Durante et al. (2018); Vozenin et al. (2019); Wilson et al. (2020b)] or when multiple micro-beams  
64 with diameter less than 1 mm distributed over a grid with inter-beam spacing  $\sim 3$  mm are used [Prezado  
65 and Fois (2013); Prezado et al. (2017b,a, 2018); González and Prezado (2018); Martínez-Rovira et al.  
66 (2017)]. However, the radiobiological mechanisms by which the therapeutic benefit is generated using  
67 these approaches are not entirely understood.

68 LhARA, the Laser-hybrid Accelerator for Radiobiological Applications, is conceived as the new, highly  
69 flexible, source of radiation that is required to explore the mechanisms by which the biological response to  
70 ionising radiation is determined by the physical characteristics of the beam. A high-power pulsed laser  
71 will be used to drive the creation of a large flux of protons or ions which are captured and formed into a  
72 beam by strong-focusing plasma lenses. The plasma (Gabor) lenses provide the same focusing strength  
73 as high-field solenoids at a fraction of the cost. Rapid acceleration will be performed using a fixed-field  
74 alternating-gradient accelerator (FFA), thereby preserving the unique flexibility in the time, energy, and  
75 spatial structure of the beam afforded by the laser-driven source.

76 The LhARA facility may be developed in two stages. In the first stage, the laser-driven beam, captured  
77 and transported using plasma lenses and bending magnets, will serve a programme of *in vitro* radiobiology  
78 with proton beams of energy of up to 15 MeV. In stage two, the beam will be accelerated using an FFA. This  
79 will allow experiments to be carried out *in vitro* and *in vivo* with proton-beam energies of up to 127 MeV.  
80 Ion beams (including  $C^{6+}$ ) with energies up to 33.4 MeV per nucleon will also be available.

81 The laser pulse that initiates the production of protons or ions at LhARA may be triggered at a repetition  
82 rate of up to 10 Hz. The time structure of the beam may therefore be varied to interrupt the chemical  
83 and biological pathways that determine the biological response to ionising radiation using 10 ns to 40 ns  
84 long proton or ion bunches repeated at intervals as small as 100 ms. The technologies chosen to capture,  
85 transport, and accelerate the beam in LhARA ensure that this unique capability is preserved. The LhARA  
86 beam may be used to deliver an almost uniform dose distribution over a circular area with a maximum  
87 diameter of between 1 cm and 3 cm. Alternatively, the beam can be focused to a spot with diameter of  
88  $\sim 1$  mm.

89 The technologies that will be developed in LhARA have the potential to make PBT available to the many.  
90 The laser-hybrid approach will allow radiobiological studies and eventually radiotherapy to be carried out

91 in completely new regimens, delivering a variety of ion species in a broad range of time structures, spectral  
92 distributions, and spatial configurations at instantaneous dose rates up to and potentially significantly  
93 beyond the current ultra-high dose-rate “FLASH” regime.

94 The “pre Conceptual Design Report” (pre-CDR) for LhARA [The LhARA consortium (2020)] lays the  
95 foundations for the development of full conceptual and technical designs for the facility. The pre-CDR  
96 also contains a description of the R&D that is required to demonstrate the feasibility of critical LhARA  
97 components and systems. This paper presents a summary of the contents of the pre-CDR and lays out the  
98 vision of the LhARA consortium.

99

## 2 MOTIVATION

100 RT delivered using protons and ions, PBT, has the potential to overcome some of the fundamental limitations  
101 of X-rays in cancer treatment through the targeted delivery of the radiation dose [Loeffler and Durante  
102 (2013)]. The Particle Therapy Co-Operative Group (PTCOG) currently lists 90 proton therapy facilities  
103 and 12 carbon ion therapy facilities worldwide, located predominantly in high-income countries [PTCOG  
104 (2020)]. Low- and middle-income countries (LMIC) are relatively poorly served, indeed nearly 70% of  
105 cancer patients globally do not have access to RT [Datta et al. (2019)].

### 106 **The case for a systematic study of the radiobiology of proton and ion beams**

107 The efficacy of proton and ion beams is characterised by their relative biological effectiveness (RBE) in  
108 comparison to a reference photon beam. The treatment-planning software that is in use in the clinic today  
109 assumes an RBE value for protons of 1.1 [Paganetti and van Luijk (2013)], meaning that, compared to  
110 X-rays, a lower dose of protons is needed to produce the same therapeutic effect. However, the rapid  
111 rise in the linear energy transfer (LET) at the Bragg peak leads to significant uncertainties in the RBE.  
112 Furthermore, it is known that RBE depends strongly on many factors, including particle energy, dose, dose  
113 rate, the degree of hypoxia, and tissue type [Paganetti (2014)]. Indeed, RBE values from 1.1 to over 3 have  
114 been derived from *in vitro* clonogenic-survival assay data following proton irradiation of cultured cell lines  
115 derived from different tumours [Paganetti (2014); Chaudhary et al. (2014); Wilkens and Oelfke (2004)].  
116 RBE values of  $\sim 3$  are accepted for high-LET carbon-ion irradiation, although higher values have been  
117 reported [Karger and Peschke (2017)]. RBE uncertainties for carbon and other ion species are at least as  
118 large as they are for protons. These uncertainties can lead to an incorrect estimation of the dose required to  
119 treat a particular tumour. Overestimation can lead to the damage of healthy tissue, while an underestimate  
120 can lead to the tumour not being treated sufficiently for it to be eradicated.

121 The radiotherapeutic effect is caused largely by irreparable damage to the cell’s DNA. The spectrum of  
122 DNA damage induced within tumour cells changes in response to differences in RBE. Larger RBE values,  
123 corresponding to higher LET, can increase the frequency and complexity of DNA damage, in particular  
124 causing DNA double-strand breaks (DSB) and complex DNA damage (CDD), where multiple DNA lesions  
125 are induced in close proximity [Vitti and Parsons (2019); Carter et al. (2018)]. These DNA lesions are  
126 a major contributor to radiation-induced cell death as they represent a significant barrier to the cellular  
127 DNA-repair machinery [Vitti and Parsons (2019)]. However, a number of other biological factors contribute  
128 to varying RBE in specific tumours, including the intrinsic radio-sensitivity of the tissue, the level of  
129 oxygenation (hypoxia), the growth and re-population characteristics, and the associated tumour micro-  
130 environment. Consequently, there is still significant uncertainty in the precise radiobiological mechanisms  
131 that arise and how these mechanisms determine the impact of PBT. Detailed systematic studies of the  
132 biophysical effects of the interaction of protons and ions, under different physical conditions, with different

133 tissue types will provide important information on RBE variation and could enable enhanced patient  
134 treatment-planning algorithms to be devised. In addition, studies examining the impact of combination  
135 therapies with PBT (e.g. targeting the DNA damage response, hypoxia signalling mechanisms and also the  
136 tumour micro-environment) are currently sparse; performing these studies will therefore provide input vital  
137 to the development of future personalised patient-therapy strategies using PBT.

### 138 **The case for novel beams for radiobiology**

139 Extending the range of beam characteristics used in PBT delivery may have significant therapeutic benefits.  
140 Delivery of RT at high dose rates has led to noticeably reduced lung fibrosis in mice, reduced skin toxicity  
141 in mini-pigs, and reduced side-effects in cats with nasal squamous-cell carcinoma, effects currently thought  
142 to be mediated via local oxygen depletion [Wilson et al. (2020b,a)]. In fact, the first patient with CD30+  
143 T-cell cutaneous lymphoma has been safely treated with electrons delivered at FLASH dose rates [Bourhis  
144 et al. (2019)]. In addition, therapeutic benefit has been demonstrated with the use of multiple micro-  
145 beams [Prezado et al. (2017b)]. However, there is still significant uncertainty regarding the thresholds  
146 and the radiobiological mechanisms underlying these effects. Extensive further study both *in vitro* and in  
147 appropriate *in vivo* models is required.

148 The LhARA facility will provide access to proton and stable ion beams, provide a wide variety of  
149 temporal, spatial, and spectral fractionation schemes, and deliver reliable and reproducible biological  
150 data with fewer constraints than at current clinical centres. LhARA will allow direct radiobiological  
151 comparisons of the effects of different charged particles at different energies and dose rates and enable  
152 unique mechanistic studies (e.g. examination of the oxygen depletion hypothesis for FLASH). In addition,  
153 LhARA will enable exhaustive evaluations of RBE using more complex end-points (e.g. angiogenesis and  
154 inflammation) in addition to routine survival measurements. The ability to evaluate charged particles in  
155 conjunction with other therapies (immunotherapy and chemotherapy) and to perform *in vivo* experiments  
156 with the appropriate animal models is of great importance given the current lack of evidence in these areas.  
157 LhARA therefore has the potential to provide the radiobiological data required to improve clinical practice.

158 The simulations of LhARA presented in this document have been used to estimate the dose delivered as a  
159 function of energy for protons and carbon ions. These simulations, described in sections 3.3 and 3.4, show  
160 instantaneous particle rates of the order of  $10^9$  particles per shot can be achieved, corresponding to average  
161 dose rates of up to  $\gtrsim 120$  Gy/s for protons and  $\gtrsim 700$  Gy/s for carbon ions. These estimates are based on  
162 the baseline specifications for LhARA.

### 163 **Laser-hybrid beams for radiobiology and clinical application**

164 High-power lasers have previously been proposed as an alternative to conventional proton and carbon-ion  
165 facilities for radiotherapy [Bulanov et al. (2002); Fourkal et al. (2003); Malka et al. (2004); Ledingham  
166 et al. (2003)]. Laser-driven sources have also been proposed as the basis for electron, proton and ion-beams  
167 for radiobiology [Kraft et al. (2010); Fiorini et al. (2011); Yogo et al. (2011); Bin et al. (2012); Doria  
168 et al. (2012); Zeil et al. (2013); Masood et al. (2014); Zlobinskaya et al. (2014)]. While a number of cell  
169 irradiation experiments have been conducted with laser-accelerated ions [Doria et al. (2012); Zeil et al.  
170 (2013); Pommarel et al. (2017); Manti et al. (2017)], these have been limited in scope to a single-shot  
171 configuration. More recent projects (e.g. A-SAIL [A-SAIL Project (2020)], ELI [Cirrone et al. (2013)] and  
172 SCAPA [Wiggins et al. (2019)]) will also investigate radiobiological effects using laser-driven ion beams.  
173 These studies will also address various technological issues [Manti et al. (2017); Romano et al. (2016a);  
174 Masood et al. (2017); Chaudhary et al. (2017); Margarone et al. (2018)].

175 A beam line to provide ion-driven beams for multi-disciplinary applications, ELIMAIA (ELI Multidi-  
176 sciplinary Applications of laser-Ion Acceleration) is being brought into operation at the Extreme Light  
177 Infrastructure (ELI) [Cirrone et al. (2020); Schillaci et al. (2019)]. This beam line will include the “ELI  
178 MEDical and multidisciplinary applications” (ELIMED) beam line which will allow radiobiological inve-  
179 stigations to be carried out [Cirrone et al. (2016); Romano et al. (2016b); Milluzzo et al. (2017); Pipek et al.  
180 (2017); Milluzzo et al. (2018); Cirrone et al. (2020)]. LhARA is distinguished from this facility in that the  
181 energy at which the beam will be captured has been chosen to maximise the shot-to-shot stability of the  
182 particle flux.

183 Protons and ions at conventional facilities are captured at energies of several tens of keV. At such low  
184 energies, the mutual repulsion of the particles, the “space-charge effect”, limits the maximum instantaneous  
185 dose rate. The laser-driven source allows protons and ions to be captured at significantly higher energies,  
186 thus evading the current space-charge limit. Rapid acceleration will be performed using a fixed-field  
187 alternating-gradient accelerator (FFA), thereby preserving the unique flexibility in the time, energy, and  
188 spatial structure of the beam afforded by the laser-driven source. Modern lasers are capable of delivering a  
189 Joule of energy in pulses that are tens of femtoseconds in length at repetition rates of  $\gtrsim 10$  Hz. Laser-driven  
190 ion sources create beams that are highly divergent, have a large energy spread, and an intensity that can vary  
191 by up to 25% pulse-to-pulse [Dover et al. (2020)]. These issues are addressed in the LhARA conceptual  
192 design through the use of Gabor lenses to provide strong focusing and to allow energy selection. In addition,  
193 sophisticated instrumentation will be used in a fast feedback-and-control system to ensure that the dose  
194 delivered is both accurate and reproducible. This approach will allow multiple ion species, from proton to  
195 carbon, to be produced from a single laser by varying the target foil and particle-capture optics.

196 LhARA will prove the principle of the novel technologies required for the development of future therapy  
197 facilities. The legacy of the LhARA programme will therefore be: a unique facility dedicated to the  
198 development of a deep understanding of the radiobiology of proton and ion beams; and the demonstration  
199 in operation of technologies that will allow PBT to be delivered in completely new regimens.  
200

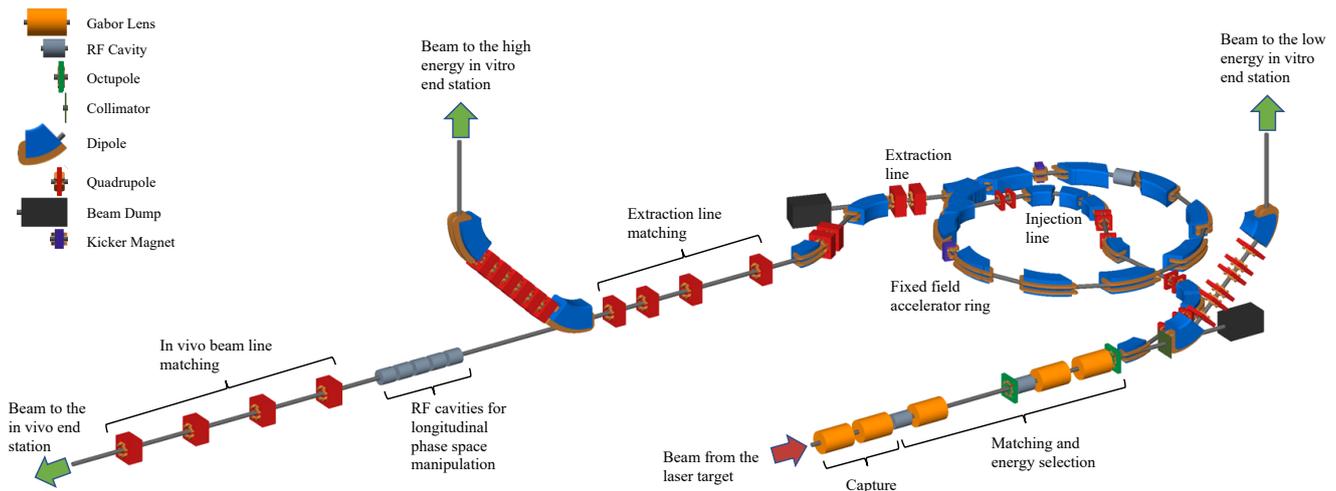
### 3 THE LHARA FACILITY

201 The LhARA facility, shown schematically in figure 1, has been designed to serve two end stations for  
202 *in vitro* radiobiology and one end station for *in vivo* studies. The principle components of Stage 1 of the  
203 LhARA accelerator are: the laser-driven proton and ion source; the matching and energy selection section;  
204 beam delivery to the low-energy *in vitro* end station; and the low-energy abort line. Stage 2 is formed by  
205 the injection line for the fixed-field alternating-gradient accelerator (FFA); the FFA; the extraction line; the  
206 high-energy abort line; beam delivery to the high-energy *in vitro* end station; and the transfer line to the *in*  
207 *vivo* end station. Proton beams with energies of between 10 MeV and 15 MeV will be delivered directly  
208 from the laser-driven source to the low-energy *in vitro* end station via a transfer line. The high-energy *in*  
209 *vitro* end station and the *in vivo* end station will be served by proton beams with energy between 15 MeV  
210 and 127 MeV and by ion beams, including  $C^{6+}$  with energies up to 33.4 MeV/u. The design parameters  
211 for the various components of LhARA are given in tables 1 and 2. The design of the LhARA facility is  
212 described in the sections that follow.

213

#### 3.1 Laser-driven proton and ion source

214 A novel solution for proton and ion acceleration is to use a compact, flexible laser-driven source coupled to  
215 a state-of-the-art beam-transport line. This allows an accelerating gradient of  $\gtrsim 10$  GV/m to be exploited  
216



**Figure 1.** Schematic diagram of the LhARA beam lines. The particle flux from the laser-driven source is shown by the red arrow. The ‘Capture’ section is followed by the ‘Matching and energy selection’ sections, the beam is directed either into the 90° bend that takes it to the low-energy *in vitro* end station, towards the FFA injection line, or to the low-energy beam dump. Post acceleration is performed using the FFA, on extraction from which the beam is directed either to the high-energy *in vitro* end station, the *in vivo* end station, or the high-energy beam dump. Gabor lenses are shown as orange cylinders, RF cavities as grey cylinders, octupole magnets as green discs, collimators as dark-green bars, dipole magnets are shown in blue, quadrupole magnets are shown in red, beam dumps (black rectangles) and kicker magnets are also shown.

217 at the laser-driven source. We propose to operate in the laser-driven sheath-acceleration regime [Clark et al.  
 218 (2000a); Snavely et al. (2000); Daido et al. (2012); Roth and Schollmeier (2016)] for ion generation. An  
 219 intense, short laser pulse will be focused onto a target. The intense electric field generated on the front  
 220 surface of the target accelerates the surface electrons, driving them into the material. Electrons which gain  
 221 sufficient energy traverse the target, ionising the material as they go. A strong space-charge electric field,  
 222 the ‘sheath’, is created as the accelerated electrons exit the rear surface of the target. This field in turn  
 223 accelerates protons and ions present as contaminants on the surface. The sheath-acceleration scheme has  
 224 been shown to produce ion energies greater than 40 MeV/u at the highest laser intensities [Dover et al.  
 225 (2020)]. The maximum proton energy ( $E_p$ ) scales with laser intensity ( $I$ ) as,  $E_p \propto I^{1/2}$ . The laser required  
 226 to deliver a significant proton flux at 15 MeV is commercially available.

227 The distribution of proton and ion energies observed in laser-driven beams exhibits a sharp cut-off at  
 228 the maximum energy and, historically, the flux of laser-accelerated ion beams has varied significantly  
 229 shot-to-shot. To reduce these variations, the choice has been made to select particles from the plateau of  
 230 the two-temperature energy spectrum of the laser-accelerated ion beam [Clark et al. (2000b); Passoni et al.  
 231 (2010)]. This should enhance ion-beam stability and allow reproducible measurements to be carried out at  
 232 ultra-high dose rates using a small number of fractions. To create the flux required in the plateau region,  
 233 it is proposed that a 100 TW laser system is used. A number of commercial lasers are available that are  
 234 capable of delivering  $> 2.5$  J in pulses of duration  $< 25$  fs, at 10 Hz with contrast better than  $10^{10} : 1$ .  
 235 Shot-to-shot stability of  $< 1\%$  is promised, an important feature for stable ion-beam production.

## 236 Target

237 Key to the operation of this configuration is a system that refreshes the target material at high repetition-rate

**Table 1.** Design parameters of the components of the LhARA facility. The parameter table is provided in a number of sections. This section contains parameters for the Laser-driven proton and ion source, the Proton and ion capture section, and the Stage 1 beam transport section.

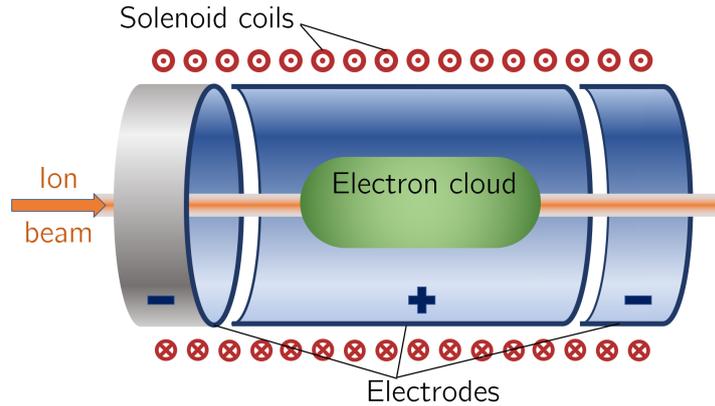
Parameter	Value or range	Unit
<b>Laser driven proton and ion source</b>		
Laser power	100	TW
Laser Energy	2.5	J
Laser pulse length	25	fs
Laser rep. rate	10	Hz
Required maximum proton energy	15	MeV
<b>Proton and ion capture</b>		
Beam divergence to be captured	50	mrad
Gabor lens effective length	0.857	m
Gabor lens length (end-flange to end-flange)	1.157	m
Gabor lens cathode radius	0.0365	m
Gabor lens maximum voltage	65	kV
Number of Gabor lenses	2	
Alternative technology: solenoid length	1.157	m
Alternative technology: solenoid max field strength	1.3	T
<b>Stage 1 beam transport: matching &amp; energy selection, beam delivery to low-energy end station</b>		
Number of Gabor lenses	3	
Number of re-bunching cavities	2	
Number of collimators for energy selection	1	
Arc bending angle	90	Degrees
Number of bending magnets	2	
Number of quadrupoles in the arc	6	
Alternative technology: solenoid length	1.157	m
Alternative technology: solenoid max field strength (to serve the injection line to the Stage 2)	0.8 (1.4)	T

238 in a reproducible manner. A number of schemes have been proposed for such studies, including high-  
 239 pressure gases [Willingale et al. (2009); Bin et al. (2015); Chen et al. (2017)], cryogenic hydrogen ribbons  
 240 [Margarone et al. (2016); Gauthier et al. (2017); Obst et al. (2017)], liquid sheets [Morrison et al. (2018)]  
 241 and tape drives [Noaman-ul Haq et al. (2017)]. For LhARA, a tape drive based on the system developed at  
 242 Imperial College London is proposed [Dover et al. (2020)]. This system is capable of reliable operation at  
 243 target thicknesses down to  $5 \mu\text{m}$ , using aluminium or steel foils, and down to  $18 \mu\text{m}$  using plastic tapes.  
 244 Such tape-drive targets can be operated at high charge (up to 100 pC at  $15 \pm 1 \text{ MeV}$ , i.e.  $> 10^9$  protons per  
 245 shot) and can deliver high-quality proton and ion fluxes at repetition rates of up to 10 Hz or greater.

246 The careful control of the tension of the tape in a tape-drive target is critical for reproducible operation.  
 247 The tape must be stretched enough to flatten the surface, but not enough to cause plastic deformations.  
 248 Surface flatness is important for a number of reasons. Rippling of the front surface modifies the laser  
 249 absorption dramatically; uncharacterised rippling can make shot-to-shot variations significant and unpredi-  
 250 ctable [Noaman-ul Haq et al. (2017)]. Similarly, rear surface perturbations can modify the sheath field,  
 251 resulting in spatial non-uniformities of the proton beam or suppression of the achievable peak energies.  
 252 Tape drives with torsion control and monitoring to maintain a high-quality tape surface have been designed  
 253 and operated in experiments at Imperial College London. The development of these targets continues with  
 254 a view to the production of new, thinner tapes for improved ion generation and the creation of ion species

**Table 2.** Design parameters of the components of the LhARA facility. The parameter table is provided in a number of sections. This section contains parameters for the Stage 2 beam transport and the *in vitro* and *in vivo* end stations.

Parameter	Value or range	Unit
<b>Stage 2 beam transport:</b> FFA, transfer line, beam delivery to high-energy end stations		
Number of bending magnets in the injection line	7	
Number of quadrupoles in the injection line	10	
FFA: Machine type	single spiral scaling FFA	
FFA: Extraction energy	15–127	MeV
FFA: Number of cells	10	
FFA: Orbit $R_{min}$	2.92	m
FFA: Orbit $R_{max}$	3.48	m
FFA: Orbit excursion	0.56	m
FFA: External R	4	m
FFA: Number of RF cavities	2	
FFA: RF frequency	1.46–6.48	MHz
FFA: harmonic number	1, 2 or 4	
FFA: RF voltage (for 2 cavities)	4	kV
FFA: spiral angle	48.7	Degrees
FFA: Max B field	1.4	T
FFA: k	5.33	
FFA: Magnet packing factor	0.34	
FFA: Magnet opening angle	12.24	degrees
FFA: Magnet gap	0.047	m
FFA: Ring tune (x,y)	(2.83,1.22)	
FFA: $\gamma_T$	2.516	
FFA: Number of kickers	2	
FFA: Number of septa	2	
Number of bending magnets in the extraction line	2	
Number of quadrupoles in the extraction line	8	
Vertical arc bending angle	90	Degrees
Number of bending magnets in the vertical arc	2	
Number of quadrupoles in the vertical arc	6	
Number of cavities for longitudinal phase space manipulation	5	
Number of quadrupoles in the <i>in vivo</i> beam line	4	
<b><i>In vitro</i> biological end stations</b>		
Maximum input beam diameter	1-3	cm
Beam energy spread (full width)	Low-energy end station: $\leq 4$ High-energy end station: $\leq 1$	% %
Input beam uniformity	$< 5$	%
Scintillating fibre layer thickness	0.25	mm
Air gap length	5	mm
Cell culture plate thickness	1.3	mm
Cell layer thickness	0.03	mm
Number of end stations	2	
<b><i>In vivo</i> biological end station</b>		
Maximum input beam diameter	1-3	cm
Beam energy spread (full width)	$\leq 1$	%
Input beam uniformity	$< 5$	%
Beam options	Spot-scanning, passive scattering, micro-beam	



**Figure 2.** Schematic diagram of a Penning-Malmberg trap of the type proposed for use in the Gabor lenses to be used in LhARA. The solenoid coils, and the direction of current flow, are indicated by the red circles (the central dots indicate current emerging from the picture, crosses current entering it). The confining electrostatic potential is provided using a central cylindrical anode and two cylindrical negative end electrodes. The ion beam enters on-axis from the left and the electron cloud is indicated by the green shaded area.

255 other than protons and carbon. This is an active area of R&D that will continue with the development of  
 256 LhARA.

257

### 258 3.2 Proton and ion capture

259 The use of an electron cloud as a focusing element for charged-particle beams was first proposed by  
 260 Gabor [Gabor (1947)]. The electron cloud is confined within the lens using a long cylindrical anode placed  
 261 within a uniform solenoid field, see figure 2. Such a configuration is commonly known as a ‘Penning  
 262 trap’ and has found wide application in many fields [Thompson (2015)]. Variations on the Penning trap  
 263 where axial apertures in the cathodes are introduced, such as the Penning-Malmberg trap [deGrassie and  
 264 Malmberg (1980); Malmberg et al. (1988)] are attractive for beam-based applications due to the excellent  
 265 access provided to the plasma column.

266 The focal length of a Gabor lens of length  $l$  is given in terms of the electron number density by:

$$\frac{1}{f} = \frac{e^2 n_e}{4\epsilon_0 U} l; \quad (1)$$

267 where  $e$  is the magnitude of the electric charge of the electron,  $n_e$  is the number density of the electrons  
 268 confined within the lens,  $\epsilon_0$  the permittivity of free space, and  $U$  the kinetic energy of the particle beam.  
 269 The desired focusing strength determines  $n_e$  which in turn allows the anode voltage and magnetic-field  
 270 strength to be calculated [Reiser (1989); Pozimski and Aslaninejad (2013)]. The focal lengths required to  
 271 capture the proton and ion beams at LhARA have been chosen such that the necessary electron number  
 272 densities lie well within the range achieved in published experiments.

273 For a given focal length, the magnetic field strength required in the Gabor lens is smaller than that of  
 274 a solenoid that would give equivalent focusing. In the non-relativistic approximation, the relationship  
 275 between the magnetic field strength in the Gabor lens,  $B_{\text{GBL}}$ , and the equivalent solenoid,  $B_{\text{sol}}$ , is given

276 by [Pozimski and Aslaninejad (2013)]:

$$B_{\text{GBL}} = B_{\text{sol}} \sqrt{Z \frac{m_e}{m_p}}; \quad (2)$$

277 where  $Z$  is the charge state of the ions. In the case of a proton beam, the reduction factor is 43. This means  
278 the cost of the solenoid for a Gabor lens can be significantly lower than the cost of a solenoid of equivalent  
279 focusing strength.

280 Instability of the electron cloud is a concern in the experimental operation of a Gabor lens; azimuthal  
281 beam disruption due to the diocotron instability has been observed and described theoretically [Meusel et al.  
282 (2013)]. Theory indicates that the diocotron instability is most problematic under well-defined geometric  
283 conditions. The reliable operation of a Gabor lens in a regime free from this instability has yet to be  
284 demonstrated. Gabor lenses promise very strong focusing, simple construction, and low magnetic field,  
285 all attractive features for LhARA. However, these attractive features come at the cost of relatively high  
286 voltage operation ( $\gtrsim 50$  kV) and possible vulnerability to instability.

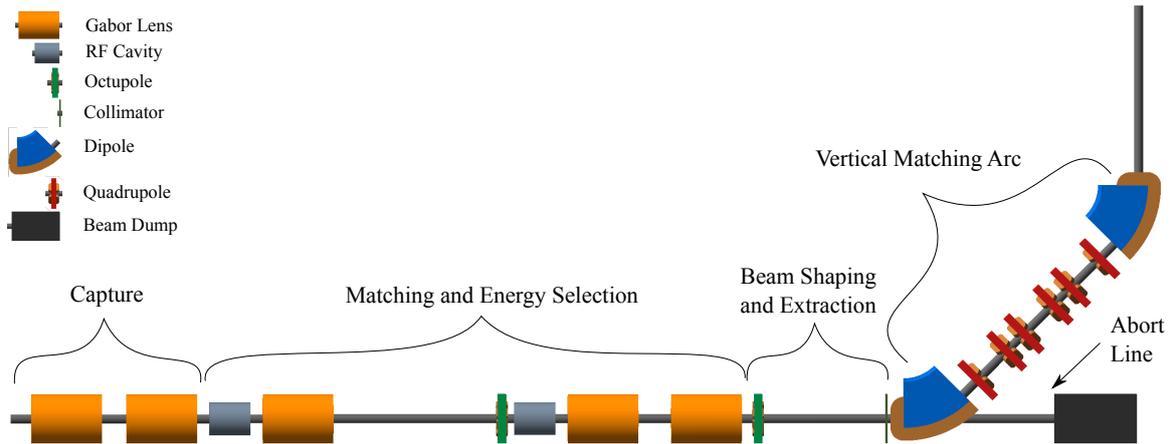
287 With reliable operation of Gabor lenses as yet unproven, we plan a two-part experimental and theoretical  
288 programme of research to investigate their suitability. Initial work will include: the theoretical study of lens  
289 stability using a full 3D particle-in-cell code such as VSIM [TECH-X (2020)]; and the development of  
290 electron-density diagnostics based on interferometric measurement of the resulting refractive-index change.  
291 A test Gabor lens will be constructed to allow validation of both the simulation results and a new diagnostic  
292 tool using an alpha emitter as a proxy for the LhARA beam. In addition, the initial investigation will  
293 include the design of an injection system to fill the lens with the required electron cloud. Should it prove  
294 impossible to produce a suitable Gabor lens, it will be necessary to use high-field solenoids to produce the  
295 equivalent focusing effect.

296

### 297 **3.3 Beam transport and delivery to the low-energy *in vitro* end station**

298 The beam transport line to the low-energy *in vitro* end station must produce a uniform dose distribution at  
299 the cell layer. Beam losses must be minimised for radiation safety and to maximise the dose that can be  
300 delivered in a single shot. The transport line has been designed to minimise regions in which the beam  
301 is brought to a focus to reduce the impact of space-charge forces on the beam phase-space. An optical  
302 solution was initially developed using Beamoptics [Autin et al. (1998)] and MADX [Grote and Schmidt  
303 (2003)]. Accurate estimation of the performance of the beam line requires the inclusion of space-charge  
304 forces and particle-matter interactions. Performance estimation was therefore performed using Monte Carlo  
305 particle-tracking from the ion source to the end station. BDSIM [Nevay et al. (2020)], which is based on  
306 the GEANT4 toolkit, was used for the simulation of energy deposition arising from beam interactions with  
307 the material in the accelerator and the end station. GPT [De Loos and Van der Geer (1996)] was used for  
308 evaluating the full 3D impact of space-charge effects.

309 An idealised Gaussian beam was generated with a spot size of  $4 \mu\text{m}$  FWHM, an angular divergence of  
310  $50$  mrad,  $35$  fs FWHM bunch length, and an energy spread of  $1 \times 10^{-6}$  MeV. The maximum estimated  
311 bunch charge is  $1 \times 10^9$  protons. The presence of a substantial electron flux produced from the laser target  
312 compensates the high proton charge density in the vicinity of the ion-production point. To approximate the  
313 partial space-charge compensation in this region, it was assumed that co-propagating electrons would fully  
314 compensate the space-charge forces over the first  $5$  cm of beam propagation. Beyond this, the proton beam  
315 was assumed to have separated from the co-propagating electrons sufficiently for space-charge to become

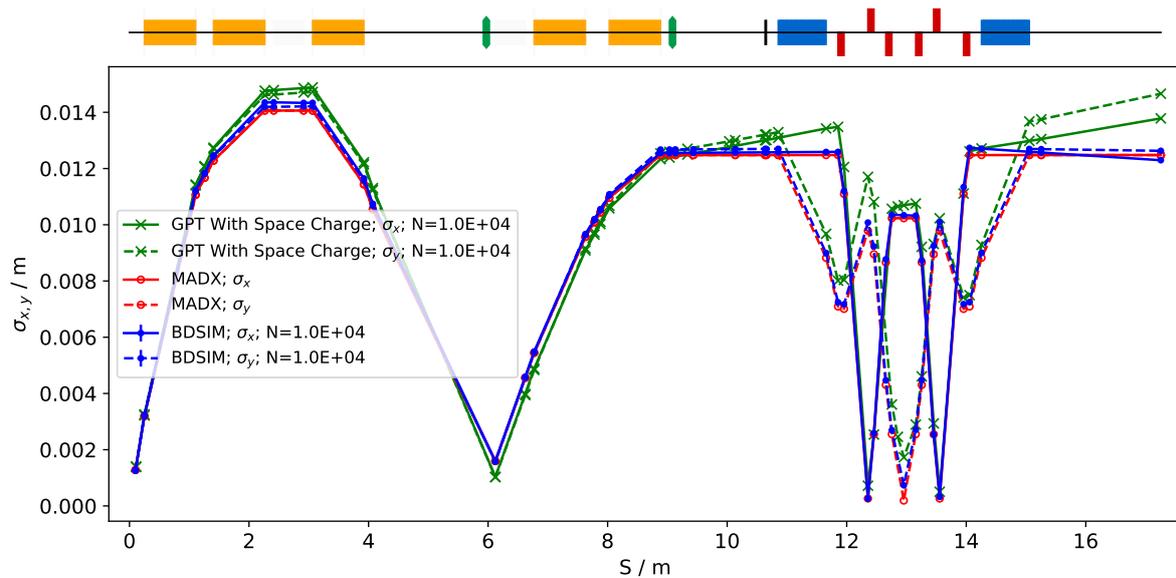


**Figure 3.** Beam transport for Stage 1 of LhARA visualised in BDSIM, showing five machine sections. The capture section is composed of two Gabor lenses (orange cylinders). The matching and energy selection section includes three Gabor lenses, two RF cavities (grey cylinders) and an octupole magnet (green disc). The beam shaping and extraction section includes a second octupole and a collimator (vertical dark-green bar). The vertical matching arc directs the beam into the low-energy *in vitro* end station and is composed of two 45° dipoles (blue and brown) and six quadrupoles (red). The total length of this beam line is 17.3 m.

316 a significant effect and cause emittance growth. Therefore, a further 5 cm drift was simulated including  
 317 space-charge forces. At a distance of 10 cm from the ion source, the beam is at the exit of the laser-target  
 318 vessel. The kinematic distributions of ions in the beam were stored at this point and passed to the relevant  
 319 BDSIM and GPT simulations of the downstream beam line.

320 The Stage 1 beam line, shown schematically in figure 3, is composed of five sections: beam capture;  
 321 matching and energy selection; beam shaping; vertical arc matching; and an abort line. The capture section  
 322 uses two Gabor lenses to minimise the transverse momentum of particles in the beam. Beyond the capture  
 323 section, an RF cavity permits control of the bunch length and manipulation of the longitudinal phase-space.  
 324 A third Gabor lens then focuses the bunch to a small spot size after which a second RF cavity is located  
 325 to provide further longitudinal phase-space manipulation. Two further Gabor lenses ensure the beam is  
 326 again parallel before it enters the vertical 90° arc. All Gabor lenses have an inner radius of 3.65 cm and an  
 327 effective length of 0.857 m. All lenses operate at a cathode voltage of less than 65 kV.

328 The parallel beam that emerges from the final Gabor lens, provides significant flexibility for the inclusion  
 329 of beam shaping and extraction systems. Beam uniformity will be achieved using octupole magnets to  
 330 provide third-order focusing to perturb the first-order focusing of the Gabor lenses. Such schemes have  
 331 been demonstrated in magnetic lattices in a number of facilities [Tsoupas et al. (1991); Urakabe et al.  
 332 (1999); Amin et al. (2018)]. A suitable position for the first octupole was identified to be after the final  
 333 Gabor lens where the beam is large; its effect on the beam is expected to be significant. Octupoles were  
 334 only modelled in BDSIM as GPT does not have a standard component with an octupolar field. The typical  
 335 rectangular transverse distribution resulting from octupolar focusing requires collimation to match the  
 336 circular aperture through which the beam enters the end station. A collimator is therefore positioned at the  
 337 start of the vertical arc. Further simulations are required to determine the optimum position of the second  
 338 octupole and to evaluate the performance of the octupoles. The switching dipole which directs the beam to  
 339 the injection line of the FFA in Stage 2 will be located between the second octupole and the collimator,  
 340 requiring the octupole to be ramped down for Stage 2 operation.



**Figure 4.** Horizontal (solid lines) and vertical (dashed lines) beam sizes through the *in vitro* beam transport, simulated including space-charge effects in GPT (green), and without space-charge in MADX (red) and BDSIM (blue).

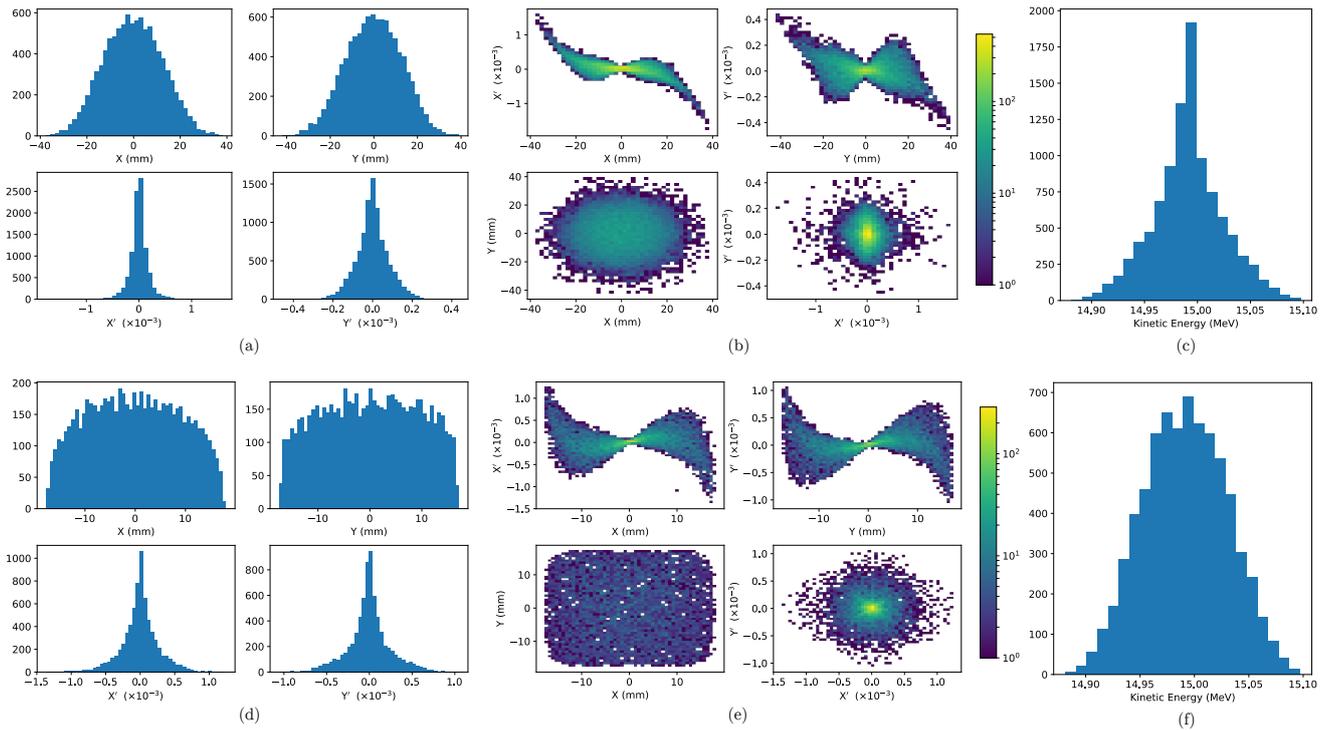
341 The vertical arc uses transparent optics in an achromat matching section to ensure that the first-order  
 342 transfer map through the arc is equivalent to the identity transformation and that any dispersive effects  
 343 are cancelled. A 2 m drift tube is added after the arc to penetrate the concrete shielding of the end station  
 344 floor and to bring the beam to bench height. The abort line consists of a drift space followed by a beam  
 345 dump. Ramping down the first vertical dipole causes the beam to enter the dump and prevents particle  
 346 transportation to the end station.

347 The underlying physics of plasma-lens operation cannot be simulated in BDSIM or GPT. It can, however,  
 348 be approximated using solenoid magnets of equivalent strength. RF cavity fields were not simulated.

349 To produce the results shown here, 10 000 particles were simulated, corresponding to the estimated  
 350 maximum bunch charge of  $1 \times 10^9$  protons. Figure 4 shows excellent agreement between horizontal and  
 351 vertical transverse beam sizes in BDSIM and MADX, verifying the beam line's performance in the absence  
 352 of space-charge effects. Reasonable agreement between BDSIM and GPT is also seen when space-charge  
 353 forces are included in GPT. Emittance growth is observed prior to the first solenoid, affecting the optical  
 354 parameters throughout the machine. However, the resulting beam dimensions at the cell layer of 1.38 cm  
 355 horizontally and 1.47 cm vertically are not significantly different from those in BDSIM. If needed, further  
 356 adjustments of the Gabor lens and arc-quadrupole strengths may compensate for any space-charge effects.  
 357 The transmission efficiency of the beam line is approximately 100%.

358 The small bunch dimensions in both transverse planes at the focus after the third Gabor lens, where  
 359 the energy selection collimator will be placed, could be of concern if the effect of space-charge has been  
 360 underestimated. Similar bunch dimensions are achieved in the vertical arc. Here, however, quadrupolar  
 361 focusing is confined to a single plane to mitigate possible further emittance growth.

362 To investigate beam uniformity, BDSIM simulations with and without octupoles and collimation for  
 363 beam shaping were conducted. Each octupole was assumed to have a magnetic length of 0.1 m and pole-tip  
 364 radius of 5 cm. The strength parameter,  $k_3$ , of each octupole was arbitrarily set to 6000. A 2 cm thick iron



**Figure 5.** Beam phase space distributions at the end-station in the transverse plane,  $(X, Y)$ ;  $X'$  and  $Y'$  give the slope relative to the  $Z$  axis. The transverse phase space is shown in figures a and b for simulations without octupolar focusing and collimation, with the kinetic energy distribution shown in c. The same phase space distributions simulated with the effect of octupoles and collimation are in figures d, e, and f.

365 collimator with a 40 mm diameter aperture was positioned 1.5 m downstream of the octupole. Figure 5  
 366 shows the beam phase-space and particle distributions at the Stage 1 end station for the transverse and  
 367 longitudinal axes with and without beam shaping. Without octupoles, the spatial profile is Gaussian, as  
 368 expected. Inclusion of the octupoles and collimation system improves beam uniformity. The total beam  
 369 width is 3.58 cm horizontally and 3.46 cm vertically, which is sufficient to irradiate one well in a six-well  
 370 cell-culture plate. Further optimisation is required to improve uniformity whilst optimising beam-line  
 371 transmission, which is approximately 70% for the results presented in figure 5.

372 An aberration can be seen in both transverse planes with and without beam shaping. This effect originates  
 373 upstream of the octupoles in the solenoids used to approximate the Gabor lenses, and persists to the  
 374 end station. The aberration is a concern, but is likely to change when the solenoids are replaced by full  
 375 electromagnetic simulation of the Gabor lenses, at which point it will be further investigated.

376 The non-Gaussian energy distribution without beam shaping is a result of space-charge forces at the  
 377 ion source; the distribution persists to the end station as no components which affect the longitudinal  
 378 phase space were simulated. The Gaussian distribution seen with beam shaping reflects the effects of the  
 379 collimation.

380 The proposed design is capable of delivering beams of the desired size to the *in vitro* end station. Space-  
 381 charge effects affect the beam-transport performance but it is believed that these can be mitigated with  
 382 minor adjustments to the Gabor lenses in the capture section. Initial studies indicate that a uniform beam  
 383 can be delivered with further optimisation of the octupoles and collimator.

384

### 385 3.3.1 Alternative Design

386 To mitigate potential emittance growth from space-charge forces, an alternative beam line design was  
387 developed in which the final two Gabor lenses in the matching and energy selection section are replaced by  
388 four quadrupoles, limiting any bunch focusing to one plane at a time. The resulting machine is reduced  
389 in length to 15.4 m. Without space-charge effects, a beam width of 2.5 mm at the end station can be  
390 achieved. With space-charge, emittance growth prior to the first solenoid is once again observed leading  
391 to an increased beam size at the entrance of the first quadrupole, resulting in a spatially asymmetric and  
392 divergent beam at the end station. It is believed that the space-charge effects can be compensated by  
393 applying the same Gabor lens optimisation as in the baseline design and adjusting the quadrupole settings  
394 to deliver beam parameters similar to those achieved in the absence of space charge. The alternative design  
395 provides a solution that is more resilient to space-charge effects than the baseline, however, only the lower  
396 bound on the desired beam size has been achieved so far. For this design, further optimisation is required  
397 not only to improve optical performance but also to optimise octupole settings and to determine whether a  
398 beam with the desired uniformity can be delivered to the end station.

399

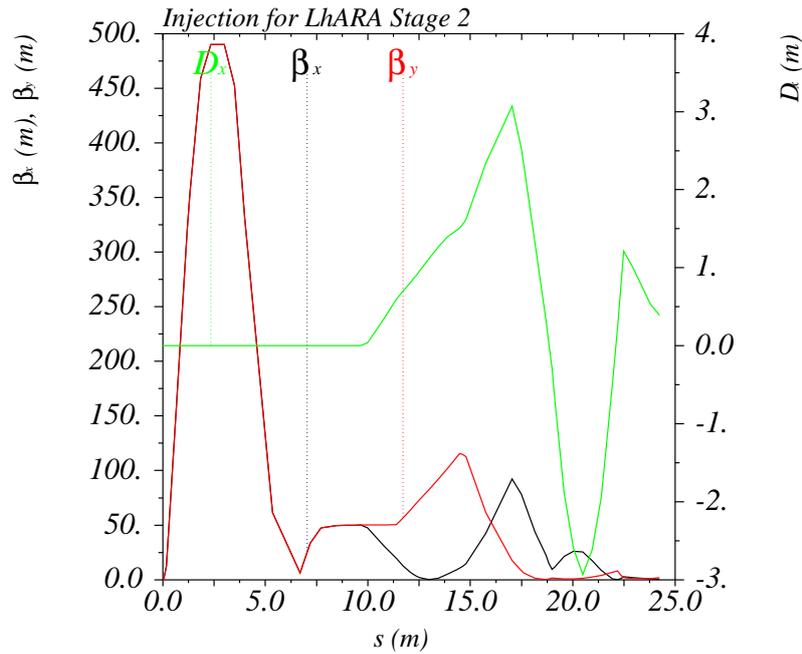
### 400 3.4 Post-acceleration and beam delivery to the *in vitro* and *in vivo* end stations

401 A fixed-field alternating-gradient accelerator (FFA), based on the spiral scaling principle [Krest et al.  
402 (1956); Symon et al. (1956); Fourier et al. (2008); Tanigaki et al. (2006)], will be used to accelerate the  
403 beam in LhARA Stage 2 to obtain energies greater than the 15 MeV protons and 4 MeV/u carbon ( $C^{6+}$ )  
404 ions delivered by the laser-driven source. FFAs have many advantages for both medical and radiobiological  
405 applications such as: the capability to deliver high and variable dose; rapid cycling with repetition rates  
406 ranging from 10 Hz to 100 Hz or beyond; and the ability to deliver various beam energies without the use  
407 of energy degraders. An FFA is relatively compact due to the use of combined function magnets, which  
408 lowers the overall cost compared to conventional accelerators capable of delivering beams at a variety of  
409 energies such as synchrotrons. Extraction can be both simple and efficient and it is possible for multiple  
410 extraction ports to be provided. Furthermore, FFAs can accelerate multiple ion species, which is very  
411 important for radiobiological experiments and typically very difficult to achieve with cyclotrons.

412 A typical FFA is able to increase the beam momentum by a factor of three, though a greater factor may  
413 be achieved. For LhARA, this translates to a maximum proton-beam energy of 127 MeV from an injected  
414 beam of 15 MeV. For carbon ions ( $C^{6+}$ ) with the same rigidity, a maximum energy of approximately  
415 33.4 MeV/u can be produced.

416 The energy at injection into the FFA determines the beam energy at extraction. The injection energy will  
417 be changed by varying the focusing strengths in the Stage 1 beam line from the capture section through to  
418 the extraction line and the FFA ring. Appropriate adjustments to the frequency and phase of the RF in the  
419 FFA ring will also be made. This will allow the required energy slice from the broad spectrum produced at  
420 the laser-driven source to be captured and transported to the FFA. The FFA will then accelerate the beam,  
421 acting as a three-fold momentum multiplier. This scheme simplifies the injection and extraction systems  
422 since their geometry and location can be kept constant.

423 A second, 'high-energy', *in vitro* end station will be served by proton beams with a kinetic energy in the  
424 range 15–127 MeV and carbon-ion beams with energies up to 33.4 MeV/u. The extraction line from the  
425 FFA leads to a 90° vertical arc to send the beam to the high-energy *in vitro* end station. If the first dipole of  
426 the arc is not energised, the beam will be sent to the *in vivo* end station. The extraction line of the FFA  
427 includes a switching dipole that will send the beam to the high-energy-beam dump if it is not energised.  
428 The detailed design of the high-energy abort line, taking into account the requirement that stray radiation



**Figure 6.** Twiss  $\beta_x$  and  $\beta_y$  functions and dispersion in the beam line consisting of the modified Stage 1 lattice and the transfer line allowing injection of the beam into the FFA ring. The distance  $s$  runs from the laser target to the exit of the injection septum.

429 does not enter the end stations, will be performed as part of the LhARA R&D programme.

430

#### 431 3.4.1 Injection line

432 In order to inject the beam into the FFA, the settings of the Stage 1 beam line need to be adjusted to reduce  
 433 the Twiss  $\beta$  function. The required Stage 1 optical parameters are shown in figure 6. The beam is diverted  
 434 by a switching dipole into the injection line which transports the beam to the injection septum magnet.  
 435 The injection line matches the Twiss  $\beta$  functions in both transverse planes and the dispersion of the beam  
 436 to the values dictated by the periodic conditions in the FFA cell (figure 6). The presence of dispersion in  
 437 the injection line allows a collimator to be installed for momentum selection before injection. The beam  
 438 is injected from the inside of the ring, which requires that the injection line crosses one of the straight  
 439 sections between the FFA magnets, see figure 7.

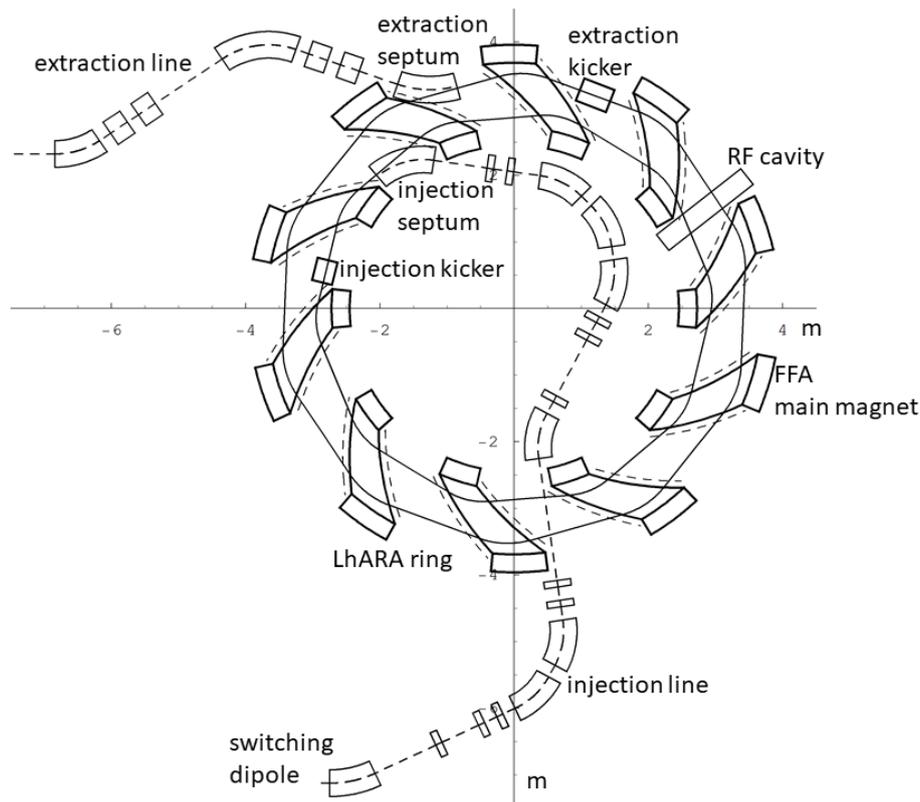
440

#### 441 3.4.2 FFA ring

442 The magnetic field,  $B_y$ , in the median plane of a scaling spiral FFA is given by [Krest et al. (1956); Symon  
 443 et al. (1956); Fourier et al. (2008)]:

$$B_y = B_0 \left[ \frac{R}{R_0} \right]^k F \left( \theta - \ln \left[ \frac{R}{R_0} \right] \tan \zeta \right); \quad (3)$$

444 where  $B_0$  is the magnetic field at radius  $R_0$ ,  $k$  is the field index,  $\zeta$  corresponds to the spiral angle and  $F$  is  
 445 the ‘flutter function’. This field law defines a zero-chromaticity condition, which means the working point



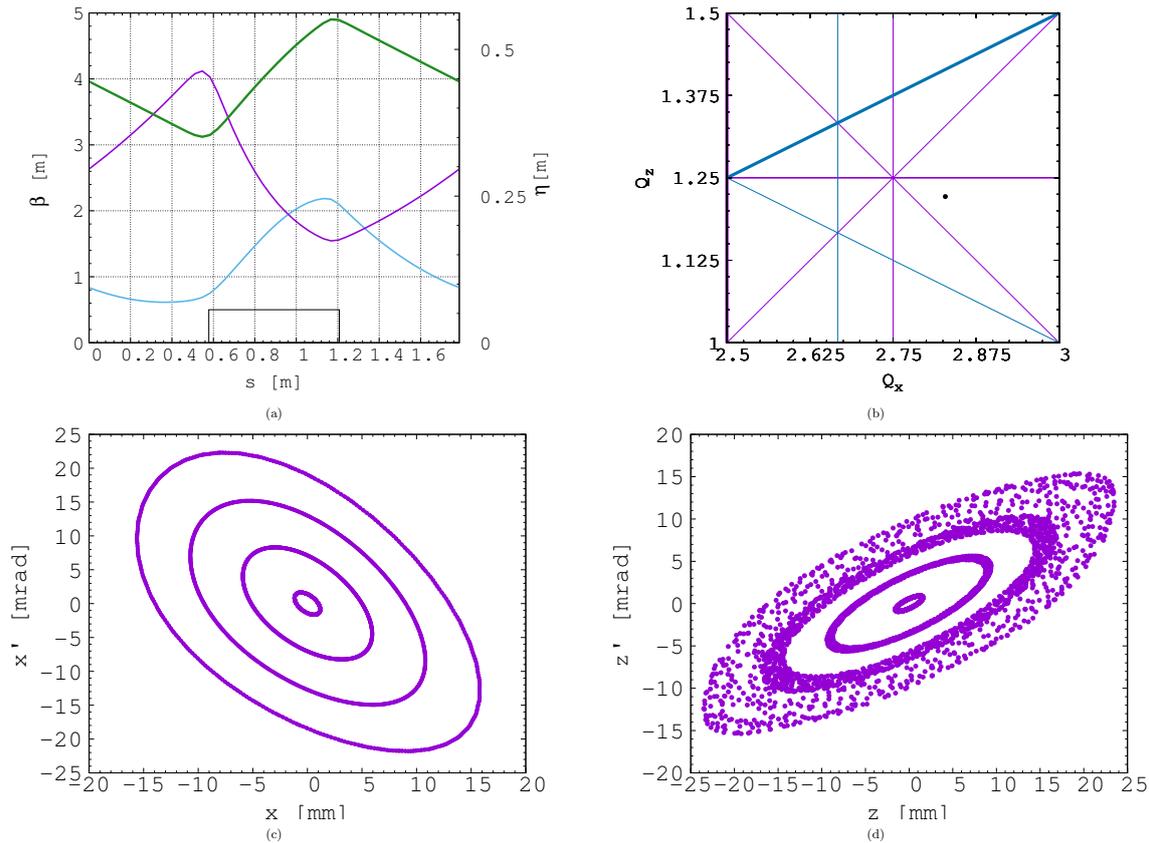
**Figure 7.** The layout of the injection line from the switching dipole to the injection septum together with the FFA ring, some of its subsystems and the first part of the extraction line.

446 of the machine is independent of energy (up to field errors and alignment imperfections). This avoids the  
 447 need to cross any resonances, which would reduce the beam quality and could lead to beam loss.

448 Table 2 gives the main design parameters of the FFA ring. The ring consists of ten symmetric cells, each  
 449 containing a single combined-function spiral magnet. The choice of the number of cells is a compromise  
 450 between the size of the orbit excursion, which dictates the radial extent of the magnet, and the length of the  
 451 straight sections required to accommodate the injection and extraction systems.

452 The betatron functions and dispersion in one lattice cell at injection are shown in figure 8(a). The tune  
 453 diagram, showing the position of the working point of the machine in relation to the main resonance lines,  
 454 is shown in figure 8(b). Tracking studies were performed using a step-wise tracking code in which the  
 455 magnetic field is integrated using a Runge-Kutta algorithm [Lagrange et al. (2018)]. The magnetic field  
 456 in the median plane was obtained using the ideal scaling law (equation 3). Enge functions were used to  
 457 give the fringe fields. The field out of the median plane was obtained using Maxwell's equations and a  
 458 6<sup>th</sup>-order Taylor expansion of the field. The dynamic acceptance for 100 turns, shown for the horizontal  
 459 and vertical planes in figures 8(c) and 8(d), respectively, is significantly larger than the beam emittance.  
 460 This statement holds even for the pessimistic scenario in which the emittance is assumed to be ten times  
 461 larger than nominal. These results confirm that a good machine working point has been chosen.

462 A full aperture, fast injection of the beam will be performed using a magnetic septum, installed on the  
 463 inside of the ring, followed by a kicker magnet situated in a consecutive lattice cell, as shown in figure 7.  
 464 The specifications of the injection system are dictated by the parameters of the beam at injection, which are  
 465 summarised for the nominal proton beam in table 3. The beam at injection has a relatively small emittance



**Figure 8.** Beam optics and tracking in the FFA. Twiss  $\beta_h$  (blue),  $\beta_v$  (purple) functions and dispersion (green) in one lattice cell of the FFA ring (a). The working point of the FFA ring at (2.83, 1.22) on the tune diagram (b). The results of the horizontal (c) and vertical (d) dynamical acceptance study in the FFA ring, where a 1 mm offset is assumed in the vertical and horizontal planes respectively.

**Table 3.** Summary of the main parameters for the proton beam at the injection to the FFA ring. These parameters correspond to the nominal (maximum) acceleration mode of operation.

Parameter	Unit	Value
Beam energy	MeV	15
Total relative energy spread	%	$\pm 2$
Nominal physical RMS emittance (both planes)	$\pi$ m rad	$4.1 \times 10^{-7}$
Incoherent space charge tune shift		-0.8
Bunching factor		0.023
Total bunch length	ns	8.1
Bunch intensity		$10^9$

466 and short bunch length, which limits the intensity accepted by the ring due to the space-charge effect. An  
 467 intensity of approximately  $10^9$  protons will be accepted by the ring assuming the nominal beam parameters.  
 468 Space-charge effects will be severe immediately after injection, but will quickly be reduced due to the  
 469 debunching of the beam. Fast extraction of the beam over the full aperture will be performed using a kicker  
 470 magnet followed by a magnetic septum installed in a consecutive lattice cell close to the extraction orbit.

471 Acceleration of the beam to 127 MeV will be done using an RF system operating at harmonic number  
 472  $h = 1$  with an RF frequency range from 2.89 MHz to 6.48 MHz. The RF voltage required for 10 Hz

**Table 4.** Beam emittance values and target  $\beta$  values for different beam sizes for 40 MeV and 127 MeV beams. The beam size is taken to be four times the sigma of the transverse beam distribution.

	40 MeV protons (Nominal)	127 MeV protons (Nominal)	127 MeV protons (Pessimistic)
RMS Emittance ( $\epsilon_x, \epsilon_y$ ) [ $\pi$ mm mrad]	0.137	0.137	1.37
$\beta$ [m] for a 1 mm spot size	0.46	0.46	0.039
$\beta$ [m] for a 10 mm spot size	46	46	4.5
$\beta$ [m] for a 30 mm spot size	410	410	40

473 operation is 0.5 kV. However, at this relatively low voltage the energy acceptance at injection is  $\pm 0.7\%$ .  
 474 Operating with a voltage of 4 kV increases the energy acceptance to  $\pm 2\%$ . This voltage can be achieved  
 475 with one cavity [Yonemura et al. (2008)]. Here, two cavities are proposed to provide greater operational  
 476 stability. Normal conducting spiral-scaling FFA magnets, similar to the ones needed for LhARA, have been  
 477 successfully constructed [Tanigaki et al. (2006); Planche et al. (2009)] using either distributed, individually-  
 478 powered coils on a flat pole piece or using a conventional gap-shaping technique. For the LhARA FFA, we  
 479 propose a variation of the coil-dominated design recently proposed at the Rutherford Appleton Laboratory  
 480 in R&D studies for the upgrade of the ISIS neutron and muon source. In this case, the nominal scaling field  
 481 is achieved using a distribution of single-powered windings on a flat pole piece. The parameter  $k$  can then  
 482 be tuned using up to three additional independently-powered windings. The extent of the fringe field across  
 483 the radius of the magnet must be carefully controlled using a ‘field clamp’ to achieve zero chromaticity.  
 484 An active clamp, in which additional windings are placed around one end of the magnet, may be used to  
 485 control the flutter function and thereby vary independently the vertical tune of the FFA ring. The FFA is  
 486 required to deliver beams over a range of energy; each energy requiring a particular setting for the ring  
 487 magnets. Therefore, a laminated magnet design may be required to reduce the time needed to change the  
 488 field. The magnet gap of 4.7 cm given in table 2 is estimated assuming a flat-pole design for the magnet.

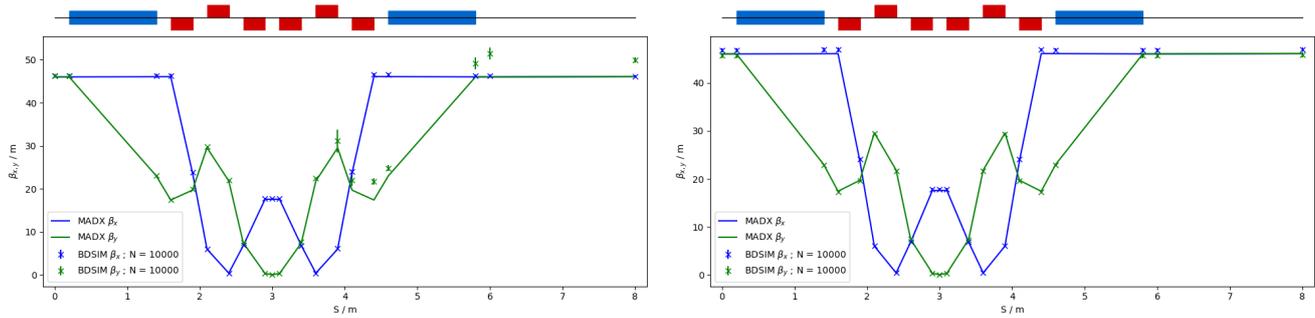
489

### 490 3.4.3 Extraction Line

491 Substantial margins in the beam parameters were assumed in the design of the extraction line from the FFA  
 492 due to uncertainties in the beam distributions originating from the Stage 1 beam transport, the FFA injection  
 493 line, and potential distortions introduced by the presence of space-charge effects during acceleration in the  
 494 ring. The beam emittance was therefore allowed to be as large as a factor of ten greater than the nominal  
 495 value, which was derived by assuming that the normalised emittance is conserved from the source, through  
 496 the Stage 1 beam line, and in the FFA ring. In the nominal case, the physical emittance of the beam is  
 497 affected by adiabatic damping only. Substantial flexibility in the optics of the extraction line is required, as  
 498 the extraction line must accommodate a wide spectrum of beam conditions to serve the *in vitro* and *in vivo*  
 499 end-stations.

500 Detailed studies were carried out for proton beams with kinetic energies of 40 MeV and 127 MeV. Table  
 501 4 gives the Twiss  $\beta$  values for different beam sizes for the 40 MeV and 127 MeV proton-beam energies  
 502 assuming a Gaussian beam distribution. The optics and geometric acceptance of the system is approximately  
 503 the same for the 40 MeV and 127 MeV beams, justifying the working hypothesis that beam emittance is  
 504 approximately the same for both beam energies. This assumption will be revised as soon as space-charge  
 505 simulations for the entire system are available.

506 The first two dipoles and four quadrupoles of the extraction line bend the beam coming from the extraction  
 507 septum of the FFA such that it is parallel to the low-energy beam line while ensuring that dispersion is



**Figure 9.** Comparison of MADX and BDSIM simulation of 40 MeV (left) and a nominal 127 MeV (right) proton beam passing through the high energy *in vitro* arc simulated with  $10^4$  particles (in BDSIM).

508 closed. Closing the dispersion is critical, as off-momentum particles will follow trajectories different to  
 509 those followed by particles with the design momentum and therefore impact the size and shape of the beam  
 510 downstream. The second part of the extraction line consists of four quadrupoles which transport the beam  
 511 either to the first dipole of the vertical arc that serves the high-energy *in vitro* end station or to the *in vivo*  
 512 end station if this dipole is not energised. These quadrupoles provide the flexibility required to produce the  
 513 different beam sizes for the *in vitro* end station, as specified in table 4.

514

#### 515 3.4.4 High-energy *in vitro* beam line

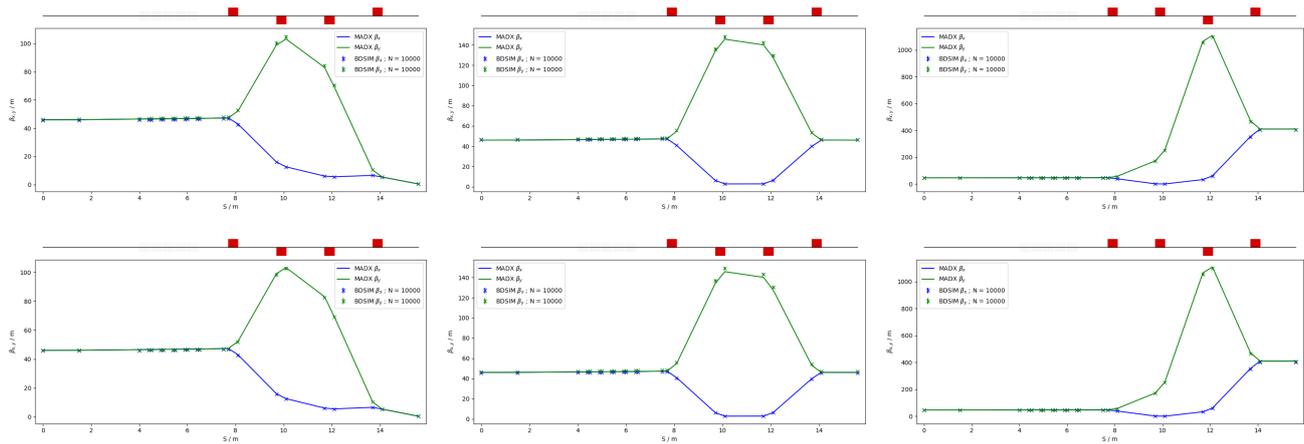
516 The high-energy *in vitro* beam line transports the beam from the extraction line to the high-energy *in*  
 517 *vitro* end station. The  $90^\circ$  vertical bend is a scaled version of the low-energy vertical arc, following the  
 518 same design principles, and also consists of two bending dipole magnets and six quadrupole magnets. To  
 519 accommodate the higher beam energies, the lengths of the magnets were scaled in order to ensure that  
 520 peak magnetic fields were below the saturation limits of normal conducting magnets. The bending dipole  
 521 magnet lengths were increased to 1.2 m each and the quadrupole lengths were tripled to 0.3 m. The overall  
 522 length of the arc then becomes 6 m, compared to 4.6 m for the low energy *in vitro* arc. This difference in  
 523 arc length means the high-energy *in vitro* arc finishes about 0.9 m higher than the low-energy one. This  
 524 difference can easily be accommodated by adjusting the final drift lengths.

525 The quadrupole strengths for the scaled high-energy *in vitro* arc were obtained using MADX calculations,  
 526 tracking simulations using BDSIM show good agreement with these, see figure 9. The input beam  
 527 distribution used in BDSIM was assumed to be Gaussian with Twiss  $\beta = 46$ , which gives a beam size  
 528 of about 10 mm. Small deviations from the BDSIM results were observed in GPT simulations due to  
 529 space-charge effects.

530

#### 531 3.4.5 *In vivo* beam line

532 To facilitate efficient small-animal handling, the end station dedicated to *in vivo* experiments will be  
 533 positioned adjacent to the principle road access to the facility. If the first dipole of the high-energy *in vitro*  
 534 arc is not energised, the beam is sent to the *in vivo* end station. From the end of the extraction line, 7.7 m of  
 535 drift is necessary to clear the first bending dipole of the *in vitro* arc, to provide space for the five RF cavities  
 536 needed for longitudinal phase-space manipulation and to allow space for diagnostic devices. Following this  
 537 drift is a further 6.6 m of beam line that includes four quadrupoles, each of length 0.4 m, which are used to  
 538 perform the final focusing adjustments of the beam delivered to the *in vivo* end station. A final 1.5 m drift  
 539 length is reserved for scanning magnets so spot scanning can be performed and to allow for penetration of  
 540 the shielding of the *in vivo* end station. In total, the *in vivo* beam line is 15.6 m in length.



**Figure 10.** MADX and BDSIM simulations of the *in vivo* beam line for a 40 MeV proton beam (top row) and a nominal 127 MeV proton beam (bottom row) with quadrupoles matched to obtain  $\beta_{x,y} = 0.46$  m (left),  $\beta_{x,y} = 46$  m (middle) and  $\beta_{x,y} = 410$  m (right) at the end of the beam line for  $10^4$  particles.

541 The flexible design can match the various  $\beta_{x,y}$  values given in table 4, but not the smallest target value of  
 542  $\beta_{x,y} = 0.039$  m for the pessimistic scenario, which is very challenging. To verify that the optics design can  
 543 provide the required beam sizes, simulations were performed with BDSIM using an input Gaussian beam  
 544 generated with the Twiss  $\beta$  values given in tables 4. Figure 10 shows the results for a 40 MeV proton beam  
 545 and a nominal emittance 127 MeV proton beam matched in order to obtain beam sizes of 1 mm, 10 mm  
 546 and 30 mm.

547

### 548 3.5 Instrumentation

549 Commercial off-the-shelf (COTS) instrumentation will be used for Stages 1 and 2 of LhARA wherever  
 550 possible. However, the characteristics of the beam (e.g. very high charge-per-bunch, low-to-moderate  
 551 energy) will require that some custom solutions be developed. The authors are developing two concepts,  
 552 termed SciWire and SmartPhantom, for the low- and high-energy *in vitro* end stations, respectively. These  
 553 detectors can also be used for beam diagnostics and may find application at other facilities. Instrumentation  
 554 for the detection of secondary particles arising from the interaction of the beam with tissue is not discussed  
 555 here but is an important area that will be studied in the future.

556

#### 557 3.5.1 SciWire

558 For the Stage 1 beam, the maximum proton energy is 15 MeV. Shot-to-shot characterisation of the beam is  
 559 essential and requires the use of a very thin detector with a fast response. The SciWire [Kurup (2019)] is  
 560 being developed to provide energy and intensity profile measurements for low-energy ion beams. A single  
 561 SciWire plane consists of two layers of  $250 \mu\text{m}$  square-section scintillating fibres, with the fibre directions  
 562 in the two layers orthogonal to each other. A series of back-to-back planes provides a homogeneous volume  
 563 of scintillator. If there are enough planes to stop the beam, the depth of penetration will allow the beam  
 564 energy to be inferred. This is a destructive measurement so would only be performed when experiments are  
 565 not running. A single plane, however, can be used for 2D beam-profile measurements while the beam is  
 566 being delivered for experiments. Light from the SciWire fibres may be detected using a CMOS camera or  
 567 photodiodes. If the instrumentation is sufficiently fast, the SciWire can be used to derive feedback signals  
 568 for beam tuning.

569

### 570 3.5.2 SmartPhantom

571 To study the dose profile of Stage 2 beams in real time, the SmartPhantom [Barber et al. (2018)] is being  
572 developed. This is a water-filled phantom, instrumented with planes of scintillating fibres, used to infer  
573 the dose distribution with distance. The detection elements of the SmartPhantom are 250  $\mu\text{m}$  diameter,  
574 round scintillating fibres. Each fibre station consists of two planes of fibres, in which the fibre directions  
575 are orthogonal. Five fibre stations are arranged in the phantom in front of the cell-culture flask. The fibres  
576 may be coupled to photodiodes, or a CMOS camera. Simulations in GEANT4 are being used to develop  
577 analysis techniques to determine the position of the Bragg peak shot-by-shot. The beam profile and dose  
578 delivered can then be calculated in real time.

579

### 580 3.5.3 Beam line Instrumentation

581 The requirement for instrumentation begins with the Ti:Sapphire laser. The laser focal spot will be  
582 characterised using a camera-based system and high-speed wavefront measurements [Wang (2014)] from  
583 COTS vendors.

584 For the Stage 1 beam line, beam position monitors (BPMs) will be needed for beam steering. Because  
585 of the low beam energy, non-intercepting BPMs using capacitive pickup buttons will be used. Custom  
586 pickups will be needed to match the beam pipe geometry, but COTS electronics are available. The beam  
587 current will be monitored near the end of each beam line, using integrating current toroids (ICT), backed  
588 up with the option of insertable multi-layer Faraday cups (MLFC) to give absolute beam current and energy  
589 measurements. Beam profiles could be measured by secondary emission monitor (SEM) grids on both  
590 Stage 1 and Stage 2 beam lines. For Stage 1, these monitors will be mounted on pneumatic actuators to  
591 avoid scattering. Each end station could be equipped with insertable “pepper-pot” emittance monitors and  
592 a transverse deflection cavity with fluorescent screen could be provided for bunch shape measurements.

593 The BPMs on the FFA will require pickup designs suitable for the unusual, wide and shallow vacuum  
594 vessel. The FFA at the KURNS facility in Kyoto has a similar layout [Uesugi (2018)] and uses a kicker and  
595 capacitive pickup to perform tune measurements in each transverse direction. A minimum of one BPM  
596 every second cell will be used in the FFA so that the beam orbit can be measured. BPMs will also be  
597 required close to the injection and extraction septa. The BPM system may be able to use COTS electronics,  
598 but the pickups will be based on the KURNS design of multiple electrodes arranged across the vacuum  
599 vessel width.

600 The data acquisition system needs to be able to store calibration data and apply corrections in real time. It  
601 is necessary to be able to find the beam centre from a profile, even when the profile may be non-Gaussian  
602 and possibly asymmetric. Field programmable gate arrays (FPGAs) can be used to perform fast fitting and  
603 pattern recognition of beam profiles. The instrumentation will be integrated with the accelerator control  
604 system and will provide fast feedback and adjustment of the beam parameters in real time.

605

### 606 3.6 Biological end stations

607 In order to deliver a successful radiobiological research programme, high-end and fully equipped *in vitro*  
608 and *in vivo* end-stations will be housed within the LhARA facility. The two *in vitro* end-stations (high  
609 and low energy) will contain vertically-delivered beam lines which will be used for the irradiation of 2D  
610 monolayer and 3D-cell systems (spheroids and patient-derived organoids) in culture. The beam line within  
611 the end-stations will be housed in sealed units that will be directly sourced with appropriate gases (carbon  
612 dioxide and nitrogen), allowing the cells within culture plates to be incubated for a short time in stable  
613 conditions prior to and during irradiation. This will also enable the chamber to act, where necessary, as a

614 hypoxia unit (e.g. 0.1%–5% oxygen concentration). Furthermore, these sealed units will contain robotics  
615 to enable the numerous cell culture plates housed within to be placed into and taken out of the beam.

616 The *in vitro* end-stations will be located within a research laboratory equipped with state-of-the-art  
617 facilities. The laboratory will include all the necessary equipment for bench-top science, sample processing  
618 and analysis (e.g. refrigerated centrifuges and light/fluorescent microscopes), along with the equipment  
619 required for contaminant-free cell culture (e.g. humidified CO<sub>2</sub> cell culture incubators, Class II biological  
620 safety cabinets), and for the storage of biological samples and specimens (e.g. –20°C and –80°C freezers  
621 and fridges). The laboratory will also house an X-ray irradiator (allowing direct RBE comparisons between  
622 conventional photon irradiation, and the proton and carbon ions delivered by the accelerator), a hypoxia  
623 chamber (for long-term hypoxia studies), a robotic workstation (for handling and processing of large sample  
624 numbers, aiding high-throughput screening experiments), and an ultra-pure-water delivery system. These  
625 facilities will enable a myriad of biological end-points to be investigated in both normal- and tumour-cell  
626 models not only from routine clonogenic survival and growth assays, but also from significantly more  
627 complex end-points (e.g. inflammation, angiogenesis, senescence and autophagy).

628 The *in vivo* end-station will be served with relatively high-energy proton and carbon ions capable of  
629 penetrating deeper into tissues allowing the irradiation of whole animals. The ability to perform *in vivo*  
630 pre-clinical studies is vital for the future effective translation of the research into human cancer patients  
631 where optimum treatment strategies and the reduction of side-effects are crucial. The *in vivo* end-station  
632 will allow the irradiation of a number of small-animal models (e.g. xenograft mouse and rat models)  
633 which can further promote an examination of particular ions on the appropriate biological end-points (e.g.  
634 tumour growth and normal tissue responses). The end-station will contain a small-animal handling area  
635 which will allow for the anaesthetisation of animals prior to irradiation. To enable the irradiation of small  
636 target volumes with a high level of precision and accuracy, an image guidance system (e.g. computed  
637 tomography) will be available. The animals will subsequently be placed in temperature-controlled holder  
638 tubes enabling the correct positioning of the relevant irradiation area in front of the beam line. The beam  
639 size is sufficient to give flexibility in the different irradiation conditions, in particular through passive  
640 scattering, pencil-beam scanning, and micro-beam irradiation, to be investigated at both conventional  
641 and FLASH dose rates. It is envisaged that the animals will be taken off-site post-irradiation to a nearby  
642 animal-holding facility for a follow-up period where biological measurements will be conducted.

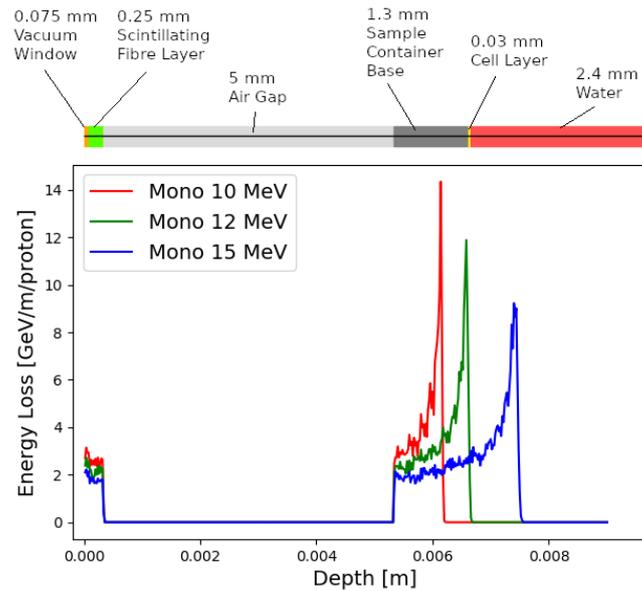
643

### 644 **3.7 Infrastructure and integration**

645 The LhARA facility will encompass two floors of roughly 42 m in length and 18 m in width. The ground  
646 floor will contain the laser, accelerator, and *in vivo* end station while the first floor will house the laboratory  
647 area and the two *in vitro* end stations. The entire facility will require radiation protection in the form  
648 of concrete shielding. There will be three principal areas: a radiation controlled-access area, a laser  
649 controlled-access area, and a laboratory limited-access area.

650 For a facility such as LhARA laser, radiation and biological safety are primary concerns. It is envisaged  
651 that LhARA will be built at a national laboratory or equivalent research institute which has an established  
652 safety-management system and culture in place.

653 The infrastructure and integration of the LhARA facility will require R&D in four key areas: risk analysis  
654 (project risks), risk assessments (safety risks), radiation simulations, and controls development. The risk  
655 analysis will cover all aspects of the facility, such as funding and resource availability, not just technical  
656 risks. A safety-risk assessment will be performed to describe and control all potential safety risks in the



**Figure 11.** Energy loss as a function of depth in the low-energy *in vitro* end station for three monoenergetic proton energies: 10 MeV; 12 MeV; and 15 MeV. Each beam was simulated using  $10^4$  particles at the start of the end station. The material through which the beam passes is indicated above the figure. The vacuum window is plotted at a depth value of 0 m. The beam deposits energy in the vacuum window and the layer of scintillating fibre before passing through an air gap and entering the sample container.

657 facility. The safety-risk assessment will, to a reasonable degree, identify all pieces of equipment that  
 658 require safety mitigations and identify control measures that must be put in place. Coupled closely with the  
 659 safety-risk assessment, radiation simulations will be developed to characterise the radiation hazards in and  
 660 around the LhARA facility. The last area to require R&D will be the control systems. It is expected that the  
 661 facility will use the Experimental Physics and Industrial Control System [The EPICS collaboration (2020)],  
 662 which can be further developed at this stage.

663

#### 4 PERFORMANCE

664 The dose distributions delivered to the end stations were evaluated using BDSIM. Figure 11 shows the  
 665 energy lost by the beam as it enters the low-energy *in vitro* end station. The beam passes through the  
 666 vacuum window, a layer of scintillating fibre, and a 5 mm air gap. The beam then enters the cell-sample  
 667 container, assumed to be polystyrene, which supports a  $30\ \mu\text{m}$  thick layer of cells, modelled using the  
 668 GEANT4 material “G4\_SKIN\_ICRP” [NIST (2017)]. The transverse momentum of protons in the beam  
 669 was assumed to follow a Gaussian distribution, with a lateral spread small enough for the beam to be fully  
 670 contained within the required spot size of 3 cm. Figure 11 shows that a proton beam with 10 MeV kinetic  
 671 energy does not reach the cell layer. The Bragg peak of a 12 MeV proton beam is located close to the cell  
 672 layer, while a 15 MeV beam, the maximum energy specified for delivery to the low-energy *in vitro* end  
 673 station, has a Bragg peak located beyond the cell layer. LhARA’s ability to deliver various beam energies  
 674 will allow the investigation of the radiobiological effects of irradiation using different parts of the Bragg  
 675 peak, effectively varying the LET across the sample. RF cavities are placed in both the stage 1 and the  
 676 stage 2 beam lines to allow the manipulation of the energy of the bunch as a function of time. This facility  
 677 will allow the study of the impact of a “spread-out Bragg peak” (SOBP).

678 The maximum dose that can be delivered was evaluated for a variety of beam energies. In order for  
679 the dose to be reported in units of Gray it is necessary to define the volume within which the energy  
680 deposition is to be integrated. Therefore, the dose was estimated from simulations by calculating the energy  
681 deposited in a volume of water corresponding in size to the sensitive volume of a PTW 23343 Markus ion  
682 chamber [GmbH (2019/2020)] placed at the position of the Bragg peak in each case. This choice allows  
683 the doses and dose-rates reported here to be compared to those of operating facilities. The cylindrical  
684 sensitive volume of the ion chamber has a radius of 2.65 mm and a depth of 2 mm, giving a volume of  
685 about  $4.4 \times 10^{-8} \text{ m}^3$ . The total energy deposited within the chamber was recorded and converted into dose  
686 in units of Gray.

687 For the low-energy *in vitro* end station, the minimum spot size has a diameter of 10 mm, which is  
688 larger than the area of the chamber. A single shot of  $10^9$  protons at 12 MeV with this spot size deposits  
689  $3.1 \times 10^{-4} \text{ J}$  in the chamber volume, corresponding to a dose of 7.1 Gy. For this simulation, the thickness  
690 of the sample container was reduced so that the Bragg peak could be positioned within the chamber volume.  
691 For the bunch length of 7.0 ns, the maximum instantaneous dose rate is  $1.0 \times 10^9 \text{ Gy/s}$  and the average  
692 dose rate is 71 Gy/s, assuming a repetition rate of 10 Hz. A single shot of  $10^9$  protons at 15 MeV deposits  
693  $5.6 \times 10^{-4} \text{ J}$  in the chamber volume, corresponding to a dose of 12.8 Gy. This gives an instantaneous dose  
694 rate of  $1.8 \times 10^9 \text{ Gy/s}$  and an average dose rate of 128 Gy/s assuming the same bunch length and repetition  
695 rate as for the 12 MeV case.

696 For the high-energy *in vitro* end station, a similar design to the low-energy end station was used, but  
697 the air gap was increased from 5 mm to 5 cm and a water phantom was placed at the end of the air gap  
698 instead of a cell culture plate. The water phantom used in the simulation was based upon the PTC T41023  
699 water phantom [PTW (2009)]. In addition, the smaller minimum design beam size of 1 mm was used. A  
700 single shot of  $10^9$  protons at 127 MeV deposits  $6.9 \times 10^{-4} \text{ J}$  in the chamber at the pristine Bragg peak  
701 depth, corresponding to a dose of 15.6 Gy, an instantaneous dose rate of  $3.8 \times 10^8 \text{ Gy/s}$  and an average  
702 dose rate of 156 Gy/s. The end-station design assumed for a 33.4 MeV/u carbon beam was the same as  
703 that used for the low-energy *in vitro* end station due to the limited range in water of the carbon beam. The  
704 intensity of the beam is assumed to be a factor of 12 less than that for protons in order to preserve the same  
705 strength of the space-charge effect at injection into the FFA with the same beam parameters because the  
706 incoherent space charge tune shift is proportional to  $q^2/A$  and inversely proportional to  $\beta^2\gamma^3$ , where  $q$  is  
707 the particle charge,  $A$  its mass number, and  $\beta$  and  $\gamma$  its relativistic parameters. A single pulse of  $8.3 \times 10^7$   
708 ions deposits  $3.2 \times 10^{-3} \text{ J}$  at the depth of the pristine Bragg peak, leading to an instantaneous dose rate of  
709  $9.7 \times 10^8 \text{ Gy/s}$  and a maximum average dose rate of 730 Gy/s.

710 The expected maximum dose rates are summarised in table 5. The instantaneous dose rates depend on the  
711 bunch length which differs depending on the energies. For the low-energy *in vitro* line, a 7 ns bunch length  
712 is assumed for all energies. For the higher energies, a 127 MeV proton beam is delivered with a bunch  
713 length of 41.5 ns, and a bunch length of 75.2 ns for a 33.4 MeV/u carbon beam. The same repetition rate of  
714 10 Hz was used for all energies. The minimum beam size at the start of the end station for the 12 MeV and  
715 15 MeV proton-beam simulations was 1 cm. A 1 mm beam size was used for the 127 MeV proton beam and  
716 33.4 MeV/u carbon-ion beam simulations.

717

## 5 CONCLUSIONS

718 The initial conceptual design of LhARA, the Laser-hybrid Accelerator for Radiobiological Applications,  
719 has been described and its performance evaluated in simulations that take into account the key features

**Table 5.** Summary of expected maximum dose per pulse and dose rates that LhARA can deliver for minimum beam sizes. These estimates are based on Monte Carlo simulations using a bunch length of 7 ns for 12 MeV and 15 MeV proton beams, 41.5 ns for the 127 MeV proton beam and 75.2 ns for the 33.4 MeV/u carbon beam. The average dose rate is based on the 10 Hz repetition rate of the laser source.

	12 MeV Protons	15 MeV Protons	127 MeV Protons	33.4 MeV/u Carbon
Dose per pulse	7.1 Gy	12.8 Gy	15.6 Gy	73.0 Gy
Instantaneous dose rate	$1.0 \times 10^9$ Gy/s	$1.8 \times 10^9$ Gy/s	$3.8 \times 10^8$ Gy/s	$9.7 \times 10^8$ Gy/s
Average dose rate	71 Gy/s	128 Gy/s	156 Gy/s	730 Gy/s

720 of the facility. LhARA uses a laser-driven source to create a large flux of protons or light ions which are  
 721 captured and formed into a beam by strong-focusing plasma lenses, thus evading prevalent space-charge  
 722 limits on the instantaneous dose rate that can be delivered. Acceleration, performed using a fixed-field  
 723 alternating-gradient accelerator, preserves the unique flexibility in the time, spectral, and spatial structure  
 724 of the beam afforded by the laser-driven source. The ability to trigger the laser pulse that initiates the  
 725 production of protons or ions at LhARA will allow the time structure of the beam to be varied to interrupt the  
 726 chemical and biological pathways that determine the biological response to ionising radiation. The almost  
 727 parallel beam that LhARA will deliver can be varied to illuminate a circular area with a maximum diameter  
 728 of between 1 cm and 3 cm with an almost uniform dose, or focused to a spot with diameter of  $\sim 1$  mm.  
 729 These features will allow radiobiological studies to be carried out in completely new regimens, delivering a  
 730 variety of ion species in a broad range of time structures and spatial configurations at instantaneous dose  
 731 rates up to and potentially significantly beyond the current ultra-high dose-rate “FLASH” regime.

732 The enhanced understanding these studies will provide, may in turn result in new approaches to radiothe-  
 733 rapy, decreasing the radio-toxicity for normal tissue while maintaining or enhancing the tumour-control  
 734 probability. Further, by developing a triggerable system that incorporates dose-deposition imaging in a fast  
 735 feedback-and-control system, in the long term LhARA has the potential to remove the requirement for a  
 736 large gantry for proton and ion therapy, laying the foundations for “best in class” treatments to be made  
 737 available to the many by reducing the footprint of future particle-beam therapy systems.

738 The radiobiology programme in combination with the demonstration in operation of the laser-hybrid  
 739 technique means that the LhARA programme has the potential to drive a step-change in the clinical practice  
 740 of proton- and ion-beam therapy.

741

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749

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