LhARA Capture Meeting

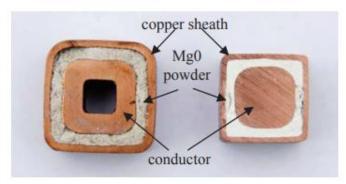
Preliminary analytical model for the LhARA solenoids

16th June 2022 Titus Dascalu

Solenoid requirements

- 1.3 T, 1 m long coil
 - $\int Bdz \leq 1.233 \text{ Tm}$ (1.2 T, 1.05 m as alternative)
- Vacuum bore ID: 60 mm
 - Limited for the 1st solenoid due to the close proximity to the target
- Coil inner radius: 38 mm
- Relatively large number of turns (e.g 4140 for 250 A)
 - Choose water-cooled hollow conductors (oxygen-free copper) to allow for higher current density j > 3 A/mm²
 - Insulation: polyimide resin + boron free glass tape (up to 1 MGy)
 - Alternative cable:
 - mineral-insulation (MgO) magnet cables, for radiation hard magnets (up to 100 MGy)
 - extensive use at PSI, JHF/J-PARC; solid/hollow conductor, nominal current up to ~ 2500 A, outward size 14-28 mm
 - direct/indirect cooling





1^{st} design iteration

Table 1: Summary specifications of the solenoid (see Section $[])$			
Parameter	Value	Units	
Maximum field strength	1.3	Т	
Coil length	1036	$\mathbf{m}\mathbf{m}$	
Coil thickness	196	$\mathbf{m}\mathbf{m}$	
Maximum coil current	250	А	
Total number of turns	4144		
Number of layers	28		
Vacuum bore ID	$60^*, 80^{**}$	mm	
Coil inner radius	$38^*, 48^{**}$	mm	
Current density	6	A/mm^2	
Hollow-conductor size	7×7	mm^2	
Conductor inner hole diameter	3	mm	
Winding bed thickness	2	mm	

Table 1. Summary specifications of the solenoid (see Section 1)

* first solenoid in the capture section

** rest of the solenoids

1st design iteration

Parameter	\mathbf{Value}^*	\mathbf{Value}^{**}	\mathbf{Units}
Coil length	3450	3710	m
Total cable mass	1293	1391	kg
Electric resistance	1.41	1.52	Ω
Power dissipated	88.2	94.9	kW
Total water flow rate	0.848	0.848	$ m Lmin^{-1}$
Water velocity	2	2	m/s
Temperature increment ^{\dagger}	53	57	°C
Reynolds number	1.2×10^4		
Pressure drop	—	—	L/s

Table 2: Other parameters of interest (see Section 2)

* first solenoid in the capture section

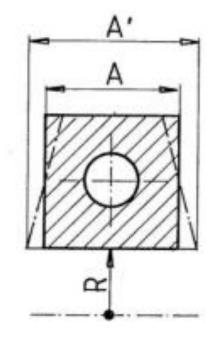
** rest of the solenoids

[†] if each layer is cooled by a separate cooling circuit

 Relatively large number of turns ⇒ large length of the cooling circuit ⇒ large temperature increment & number of cooling circuits

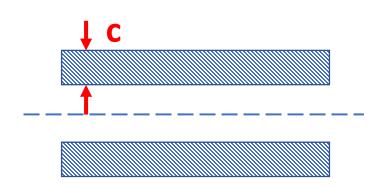
Keystone effect – an issue (?)

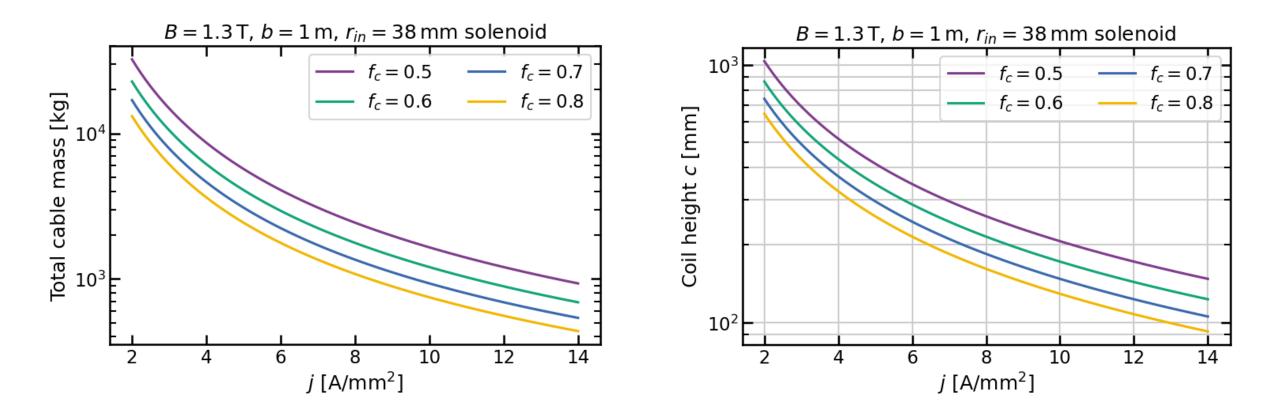
- Rule of thumb: choose a bending radius four times larger than the conductor width
 - for an inner coil radius \sim 4 cm, cable width limited to \sim 1 cm



Scaling studies: magnet size

• Filling factor
$$f_c = \frac{\text{net conductor area}}{\text{coil cross section}}$$
 (typically $0.6 \le f_c \le 0.8$)





Space constraints for the 1^{st} solenoid in the beamline

CERN Summer Student Programme 2021 Report

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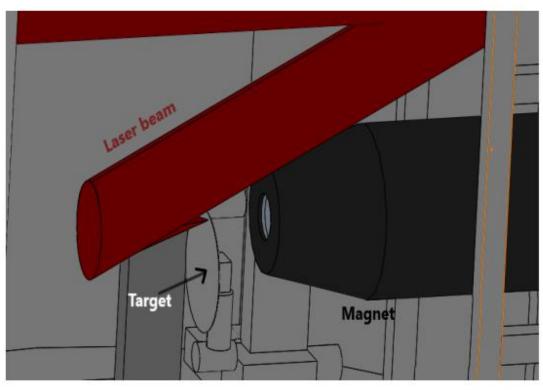
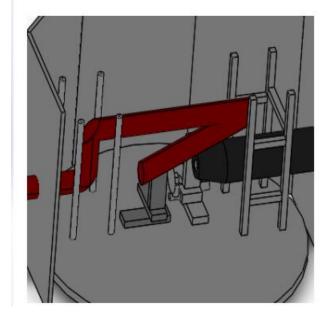
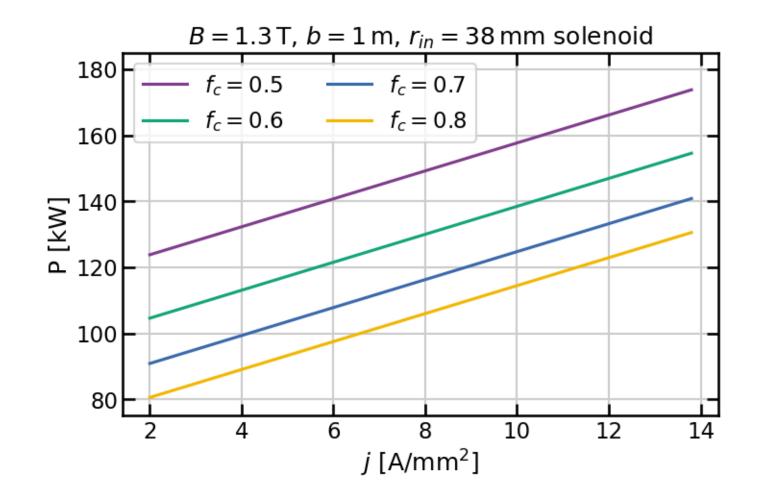


Figure 2 – Minimum distance between the magnet and the target



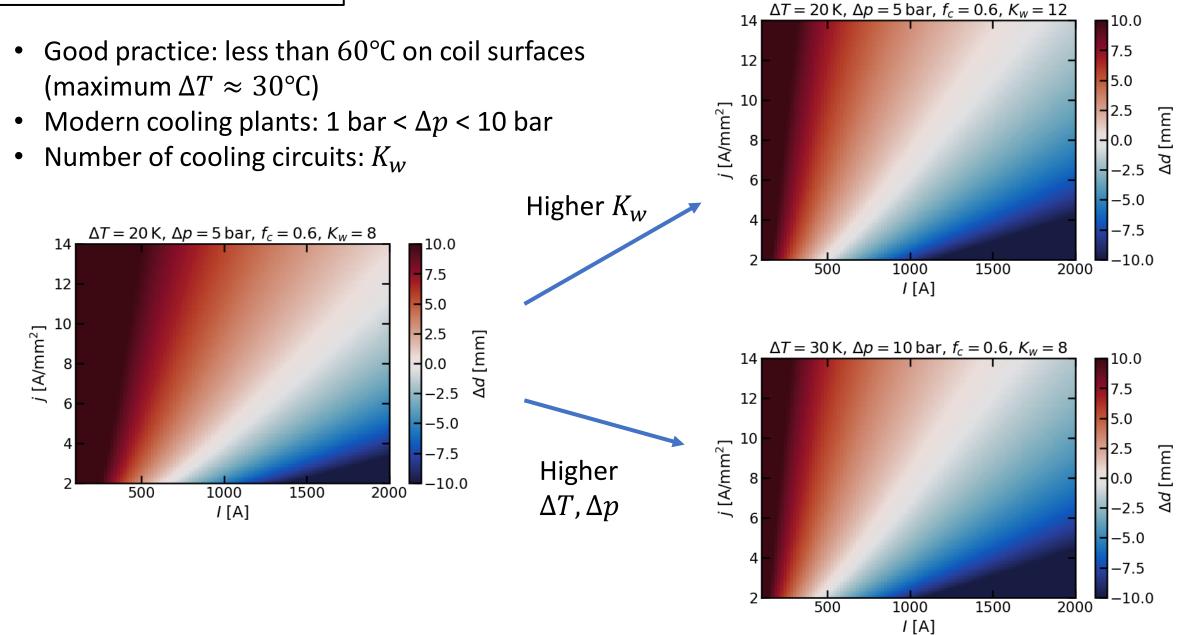
- Solenoid OD < 150 mm
 - For magnet entrance to be placed 150 mm from target

Scaling studies: power



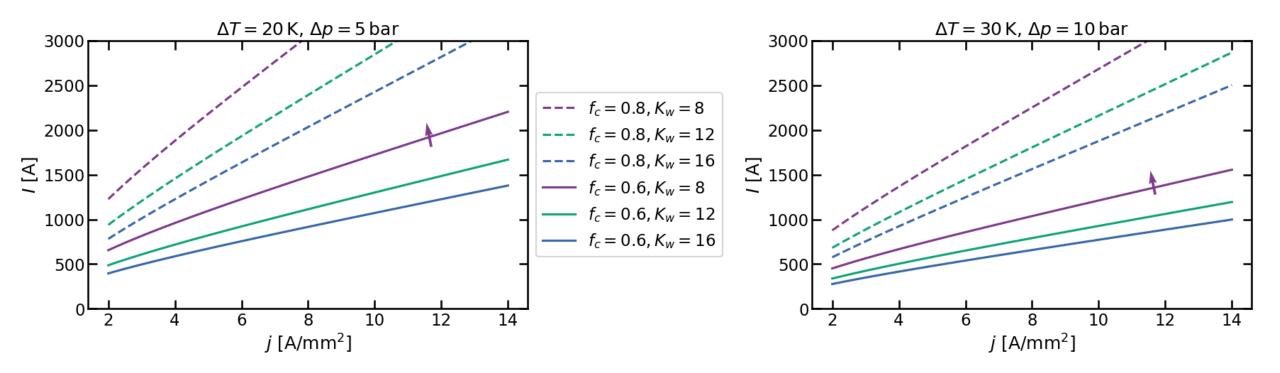
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Cooling requirements



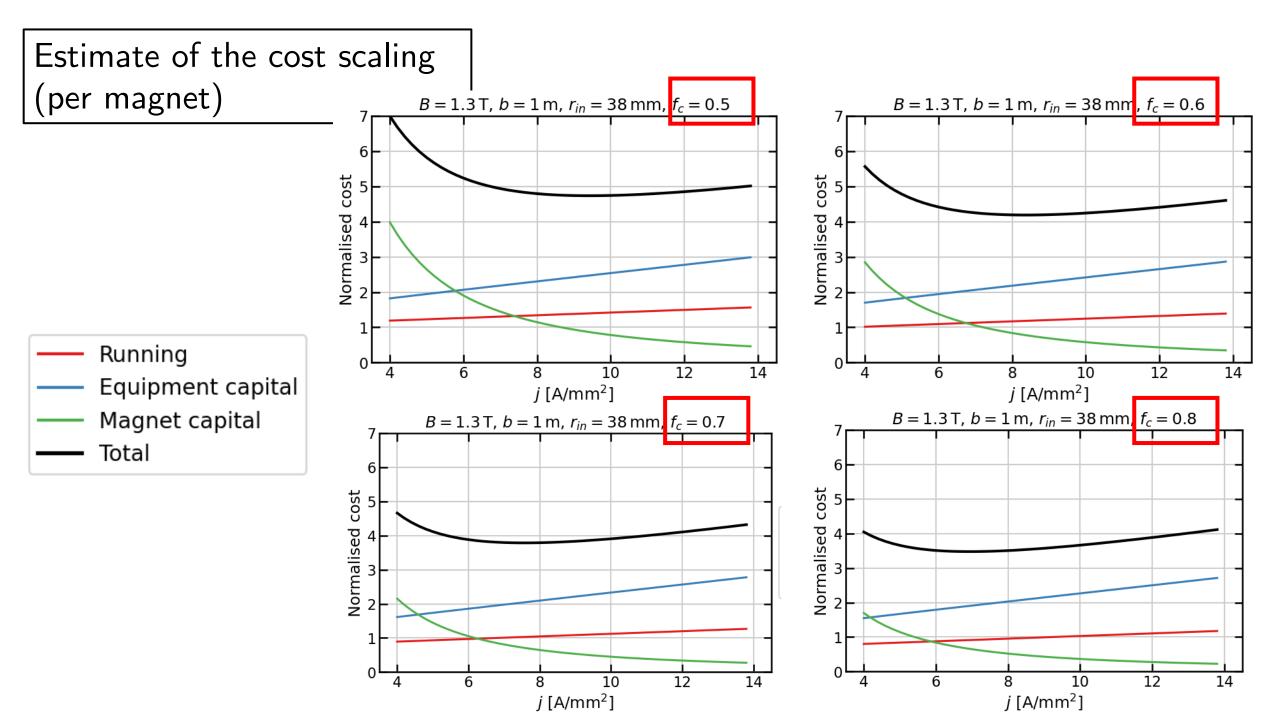
Cooling requirements

- Keeping the water temperature down constraints the area needed for the cooling pipe
 - For fixed j, f_c the constraint propagates into the current which must be chosen on/above the lines plotted below



Estimate of the cost scaling

- Cost scaling based on a procedure from:
 - G. Brianti and M. Gabriel, Basic expressions for evaluating iron core magnets A possible procedure to minimize their cost, CERN/SI/Int. DL/70-10 (1970).
 - + a few modifications to account for the increase in the power supply with the current
 - Assumption: the cost doubles when going from 250A to 1000A
- 60,000 hours of running (~ 15 years of 12 hours/day)
- Iron return yoke/cover included
- One power supply per magnet
- Equipment cost includes
 - Cost of power supply
 - Cost of d.c. power distribution
 - Cost of cooling
- Absolute cost is not specified (only the approximate relations between various cost components)



• Possible configuration near the target

